



# PARASITIC STRIP RECTANGULAR MICROSTRIP MONOPOLE ANTENNAS FOR HIPERLAN AND UWB OPERATION

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**ABSTRACT:** A low profile parasitic strip rectangular monopole microstrip antenna is proposed for HIPERLAN/2 and UWB operation. The antenna has a simple structure consisting of a rectangular radiating patch of size 2.34 X 3.04 cm<sup>2</sup> with parasitic strip and uses low cost substrate material FR4. The proposed antenna excites six resonant modes and gives a peak gain of 11.70 dB. If the radiating patch is modified by loading simple rectangular vertical slots on the patch the antenna operates for five bands of frequencies. Both the cases antennas operate in the frequencies range of 4 to 16 GHz and gives omnidirectional radiation characteristics. The proposed antenna may find application in microwave communication systems.

**Keywords:** microstrip antenna, monopole, slot, omnidirectional, parasitic strip

## I. INTRODUCTION

Emerging trends in microwave communication systems, monopole microstrip antennas are popular because of compact size, simple in design, low cost and capable of operating more than one band of frequencies. Owing to its thin profile, light weight, low cost, planar configuration and easy fabrication, the monopole microstrip antenna is the better choice for these requirements. Number of investigations have been reported in the literature an monopole microstrip antennas such as parasitic planar element for bandwidth enhancement of 1 to 9 GHz [3], band-rejected antenna with the parasitic strip for UWB [4], microstrip-fed monopole antenna with a shorted parasitic element for wideband covering Bluetooth/ISM, 2.5 GHz WiMAX, 3.5 GHz WiMAX, and 5.2/5.8 GHz WLAN [5], a triple-band CPW-fed microstrip antenna for WLAN and WiMAX [6], a new triple-band CPW-fed monopole antenna for WLAN and WiMAX [7], slotted rectangular microstrip antenna for bandwidth enhancement [8], open L-slot antenna with rotated rectangular patch for bandwidth enhancement [9] etc. But the design and development of parasitic strip monopole microstrip antenna for HIPERLAN/2 and UWB operation is rarely found in the literature. Further most of the antennas presented in the literature are either complex in their structure or bigger in size and hence require careful manufacturing procedure than that of the regular microstrip antenna for practical applications.

## II. DESIGN OF ANTENNA GEOMETRY

The art work of the proposed antenna is sketched by using computer software Auto-CAD to achieve better accuracy and is fabricated on low cost FR4-epoxy substrate material of thickness of  $h = 0.16$  cm and permittivity  $\epsilon_r = 4.4$ .

Figure 1 shows the top view geometry of parasitic strip rectangular monopole microstrip antenna (PRMA). In Fig.1 the area of the substrate is  $L \times W$  cm. On the top surface of the substrate a ground plane of height which is equal to the length of microstripline feed  $L_f$  is used on either sides of the microstripline with a gap of 0.1 cm. On the bottom of the substrate a continuous ground copper layer of height  $L_f$  is used below the microstripline. The PRMA is designed for 3 GHz of frequency using the equations available for the design of conventional rectangular microstrip antenna in the literature [2]. The length and width of the rectangular patch are  $L_p$  and  $W_p$  respectively. The feed arrangement consists of quarter wave transformer of length  $L_t$  and width  $W_t$  which is connected as a matching network between the patch and the microstripline feed of length  $L_f$  and width  $W_f$ . A semi miniature-A (SMA) connector is used at the tip of the microstripline feed for feeding the microwave power. In Fig.1 a parasitic strip is used around the radiating patch with a gap of 0.2 cm.

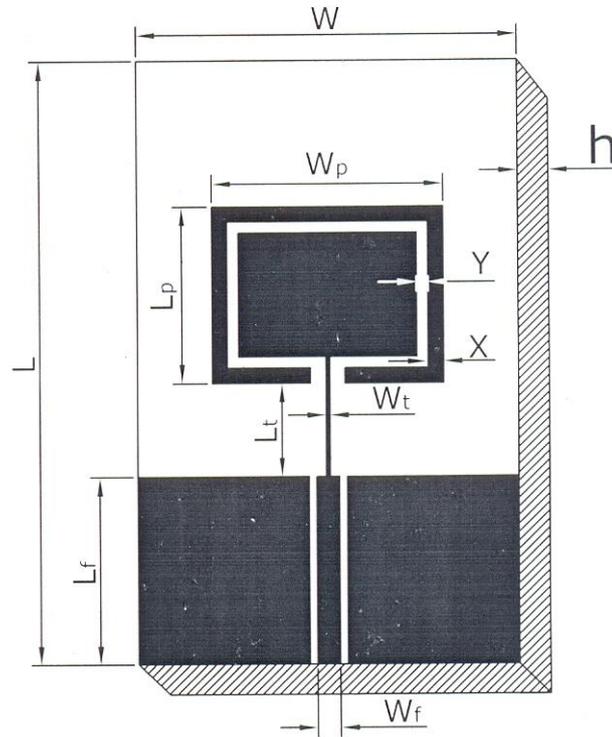


Fig. 1 Top view geometry of PRMA

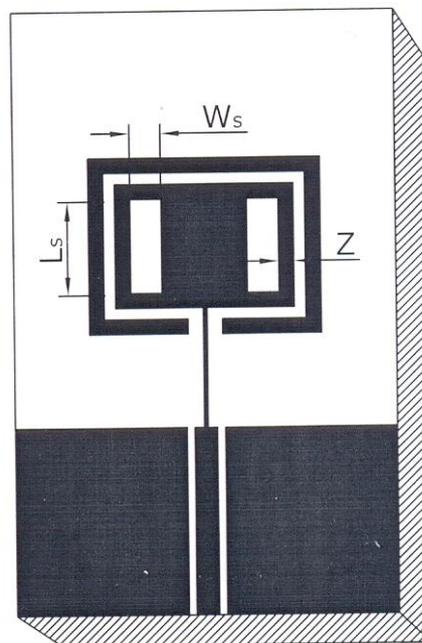


Fig. 2 Top view geometry of SPRMA

Figure 2 shows the geometry of slotted parasitic strip rectangular monopole microstrip antenna (SPRMA). In this figure rectangular slots are loaded on the radiating patch with a gap of  $Z$  (i.e.0.25 cm) from its vertical sides. The length and width of the slots are  $L_s$  and  $W_s$  respectively. The other geometry of Fig. 2 remains same as that of Fig.1. The design parameters of the proposed antenna is shown in Table 1



TABLE 1  
 DESIGN PARAMETERS OF PROPOSED ANTENNA

Antenna parameter	L	W	L <sub>p</sub>	W <sub>p</sub>	L <sub>f</sub>	W <sub>f</sub>	L <sub>t</sub>	W <sub>t</sub>	X	Y	Z	L <sub>s</sub>	W <sub>s</sub>
Dimensions in cm	8.0	5.0	2.34	3.04	2.48	0.3	1.24	0.05	0.2	0.4	0.25	1.24	0.41

III. EXPERIMENTAL RESULTS AND DISSCUSION

The antenna bandwidth over return loss less than -10 dB is tested experimentally on Vector Network Analyzer (Rohde & Schwarz, Germany make ZVK model 1127.8651). The variation of return loss verses frequency of PRMA is as shown in Fig. 4. From this graph the experimental bandwidth (BW) is calculated using the equations,

$$BW = \left[ \frac{f_2 - f_1}{f_c} \right] \times 100 \% \tag{1}$$

were, f<sub>1</sub> and f<sub>2</sub> are the lower and upper cut of frequencies of the band respectively when its return loss reaches – 10 dB and f<sub>c</sub> is the centre frequency of the operating band. From this figure, it is found that, the antenna operates between 4 to 16 GHz and gives six resonant modes at f<sub>1</sub> to f<sub>6</sub>, i.e. at 4.74, 6.30, 8.92, 12.97, 14.07 and 15.27 GHz. The magnitude of experimental -10 dB bandwidth measured for BW<sub>1</sub> to BW<sub>6</sub> by using the equation (1) is found to be 90 MHz (1.47 %), 1.11GHz (17.68 %), 1.56 GHz (16.93 %), 3.26 GHz (27.62 %), 960 MHz (6.74 %) and 760 MHz GHz (4.80 %) respectively. From Fig.2 it is clear that, the operating band BW<sub>2</sub> covers HIPERLAN/2 i.e. from 5.72 to 6.83 GHz.

The resonant mode at 4.78 GHz is due to the fundamental resonant frequency of the patch and others modes are due to the novel geometry of PRMA. The multi mode response obtained is due to different surface currents on the patch. The fundamental resonant frequency mode shifts from 3 GHz designed frequency to 4.78 GHz due to the coupling effect of microstripline feed and top ground plane of PRMA.

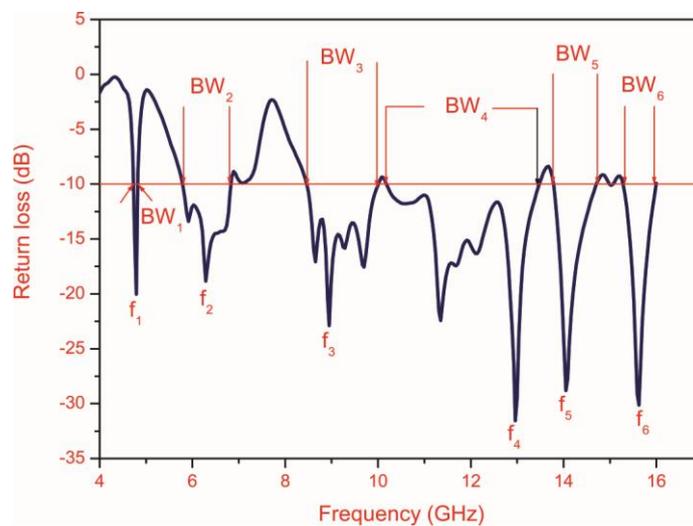


Fig. 3 Variation of return loss versus frequency of PRMA

Figure 4 shows the variation of return loss verses frequency of SPRMA. It is seen from this figure that, the antenna operates for five bands of frequencies BW<sub>7</sub> to BW<sub>11</sub>. The magnitude of these operating bands measured at BW<sub>7</sub> to BW<sub>11</sub> is found to be 140 MHz (2.93 %), 930 MHz (14.77 %), 250 MHz (3.45 %), 1.46 GHz (15.88), and 5.59 GHz (42.33 %) respectively. From Fig. 4 it is seen that the f<sub>4</sub>, f<sub>5</sub>, and f<sub>6</sub> of BW<sub>4</sub>, BW<sub>5</sub> and BW<sub>6</sub> of Fig.3 are merged together into a single band BW<sub>11</sub> in this as shown in Fig.4. Further from Fig.4 it is clear that, the SPRMA is capable of widening its operating bands when compared to the operating bands of PRMA. Hence by controlling the location and dimension of slots on the patch antenna can be made to operate for desired frequency range.

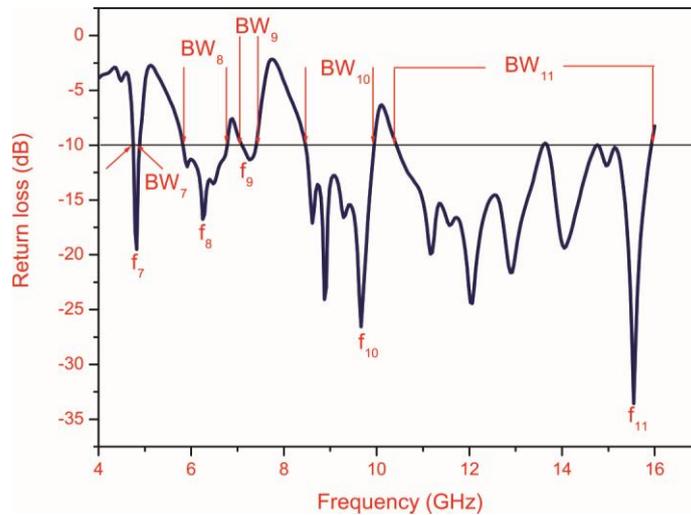


Fig. 4 Variation of return loss versus frequency of SPRMA

The gain of the proposed antennas is measured by absolute gain method. The power transmitted ‘ $P_t$ ’ by pyramidal horn antenna and power received ‘ $P_r$ ’ by antenna under test (AUT) are measured independently. With the help of these experimental data, the gain (G) dB of AUT is calculated by using the formula,

$$(G) \text{ dB} = 10 \log \left( \frac{P_r}{P_t} \right) - (G_t) \text{ dB} - 20 \log \left( \frac{\lambda_0}{4\pi R} \right) \text{ dB} \quad (2)$$

where,  $G_t$  is the gain of the pyramidal horn antenna and R is the distance between the transmitting antenna and the AUT. Using equation (2), the peak gain of the proposed antennas measured in their operating bands is found to be 11.70 dB and 9.54 dB respectively.

The co-polar and cross-polar radiation pattern of PRMA and SPRMA is measured at 4.74 GHz and are shown in Fig 5 to 6 respectively. The obtained patterns are omnidirectional in nature

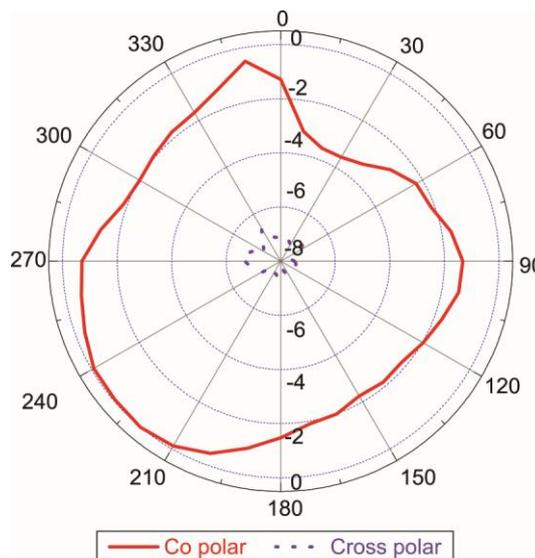


Fig. 5 Radiation pattern of PRMA measured at 4.74 GHz

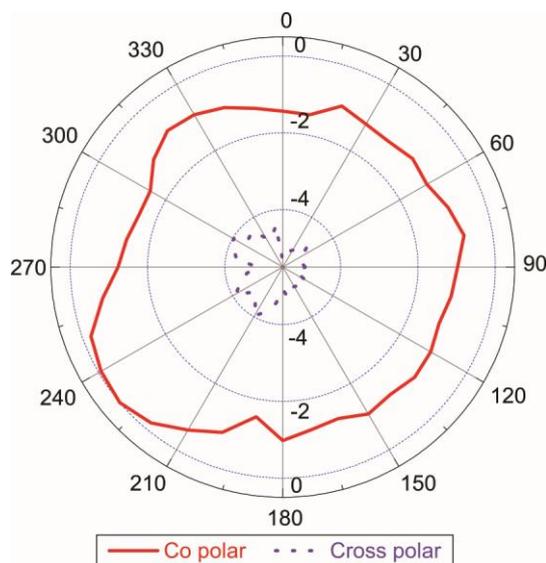


Fig. 6 Radiation pattern of SPRMA measured at 4.74 GHz

#### IV.CONCLUSION

From the detailed experimental study, it is concluded that, the PRMA with microstripline feed is useful for HIPERLAN/2 (BW<sub>2</sub> i.e. 5.72 to 6.83 GHz) and UWB applications. The antenna has simple structure which consists of a rectangular radiating patch of 2.34 X 3.04 cm<sup>2</sup> with parasitic strip and use low cost substrate material FR4. The proposed antenna excites six resonant modes and gives peak gain of 11.70 dB. Further if the radiating patch is modified by loading rectangular vertical slots on the patch and antenna operates for five wide operating bands. In both the cases antenna operates in the frequencies range of 4 to 16 GHz and gives omnidirectional radiation characteristics. The proposed antennas may find application in HIPERLAN/2 and microwave communication systems.

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### BIOGRAPHY



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