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# A New Hybrid Dual Input DC–DC Converter with P&O Algorithm Employing MPPT for Renewable Energy Applications

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**ABSTRACT:** This paper, going to propose a new hybrid dual input DC-DC Converter with P&O algorithm employing MPPT for renewable energy applications. The major disadvantage of conventional single input hybrid DC-DC converters is its inconsistency in nature. Here we are introducing a new DC-DC converter with dual input. The proposed converter is basically a modified version of hybrid Sepic-Cuk converter i.e., a combination of basic Sepic converter and Cuk converter. The new hybrid dual input DC-DC Converter can produce a constant output. Solar photovoltaic panel (SPV) and fuel cell are connected to the two input terminals of the new converter. The outputs of both the converters are integrated to single section. If the availability of the sunlight is decreased due to worst climatic condition or during night time, the fuel cell can compensate the output voltage. The circuit also have an advantage of individual and simultaneous operation. This system finds applications in remote area power generation, constant speed energy conversion systems, variable speed energy conversion systems, rural electrification, water pumping system, etc. MATLAB/SIMULINK R2015a is used for simulation works. The analysis is done based on the simulation results.

**KEYWORDS:** Hybrid DC-DC converter, solar photovoltaic panel, Sepic-Cuk converter, water pumping system.

## I.INTRODUCTION

The demand for energy increases day by day. But now, the availability of energy decreases due to the uncontrolled utilisation of conventional energy resources. Fossil fuels are the most prominent conventional energy sources that are used to meet energy demand. Environmental pollution and hence global warming are the major impact made by fossil fuels. Also the limitation of the availability of such sources will raise the importance of renewable energy resources. These resources are environmental friendly and persist abundantly in nature. Solar energy and wind energy are the most important renewable energy resources obtained from nature. The capital cost of systems which uses renewable sources are high but the operating cost is very low. By efficient utilisation of such resources can meet the energy demand. Solar energy is the most efficient and easily available renewable energy resource. One of the major issues with these renewable energy resources are its inconsistent nature, i.e., such systems will generate fluctuating output. Hybridization is the most effective technique to overcome this problem.

Armando Cordeiro, Miguel Chaves, Hiren Canacsinh, Ricardo Luis, Vitor F. Pires, Daniel Foito, A. J. Pires, Joao F. Martins[1] introduced a hybrid Sepic-Cuk DC-DC converter associated to a SRM drive for a solar PV powered water pumping system. The converter proposed in this system is a combination of a Sepic converter and a Cuk converter. Figure: 1 shows the circuit diagram of hybrid Sepic-Cuk DC-DC converter. In mode 1, the switch S is ON. Inductor,  $L_1$  starts charging. The diodes  $D_1$  and  $D_2$  are reverse biased. Capacitors  $C_1$ ,  $C_3$  and  $C_4$  start discharging the stored energy. Energy stored in the capacitor  $C_1$  discharges through the load. The capacitor  $C_4$  discharges its energy through switch S and then through inductor  $L_2$ . Now  $L_2$  starts charging. The inductor  $L_3$  and capacitor  $C_2$  are



also starts charging by the discharging of the capacitor  $C_3$ . In mode 2, the switch  $S$  is in OFF position. The diodes  $D_1$  and  $D_2$  are forward biased and starts conducting. Inductor  $L_1$  starts to discharge the energy stored in it. By this energy, the capacitors  $C_1$ ,  $C_3$  and  $C_4$  become charging condition. The inductors  $L_2$  and  $L_3$  are starts to discharge its energy. The capacitor  $C_2$  is also in discharging mode.

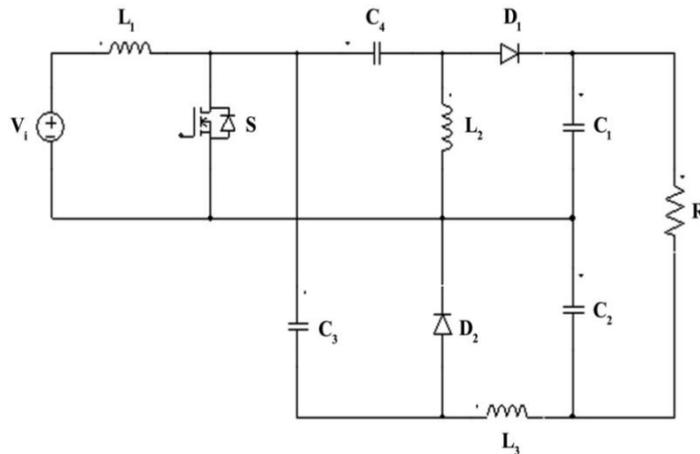


Figure. 1: Hybrid Sepic-Cuk DC-DC converter

The major disadvantage of the above system is the incapability of maintaining a constant output due to the unavailability of solar radiations during night time and due to worst climatic conditions. To overcome this drawback, a solar array - fuel cell hybrid DC-DC converter is presented.

## II. PROPOSED CONVERTER

Similar to the hybrid Sepic-Cuk DC-DC converter, the dual input DC-DC converter is also a combination of Sepic converter and Cuk converter. By combining these two converters can be eliminate separate input filters. The proposed converter consists of two input ports and the output sections of both converters are merged to single section to develop the converter topology. Solar radiation and energy stored in a fuel cell are the two inputs of the converter. Solar photovoltaic arrays (SPV) are used to extract energy from solar radiations. Maximum power point tracking (MPPT) is employed to ensure that maximum power should be transferred from source to load. For the proposed converter, perturb and observe (P&O) algorithm is used. For a fuel cell chemical energy stored is converted to electrical energy and that is used as the secondary input of the converter.

The proposed converter is capable of simultaneous or individual operation. Large amount of solar radiations are obtained during sunny days. During these days, the output from the solar photovoltaic array is sufficient to make required output. Individual operation of the converter is enough at this condition. But during rainy days or during night time solar radiations are not sufficient to meet the demand. At this time the fuel cell will act and thereby compensate the output voltage. The fuel cells can supply energy as long as the fuel and oxygen is present. Hydrogen is commonly used in fuel cells to generate chemical energy. Simultaneous operation of the converter is carried out for this situation. Constant output voltage will maintain by using this conditions. The circuit diagram of a new hybrid dual input DC-DC converter is shown in figure 2.  $V_1$  is taken as the solar array voltage and  $V_2$  as the fuel cell voltage.  $M_1$  and  $M_2$  are the switches in the Cuk section and Sepic section of the circuit respectively.  $L_1$  and  $C_1$  are the input inductor and coupling capacitor of the Cuk converter section. Similarly,  $L_3$  and  $C_3$  are the input inductor and coupling capacitor of the Sepic converter section. Diodes  $D_1$  and  $D_2$  of the converters are reconfigured in this circuit.  $L_2$  and  $C_2$  are the output inductor and output capacitor of the converter.  $R$  is the load resistor. A constant voltage is obtained across the load resistor.

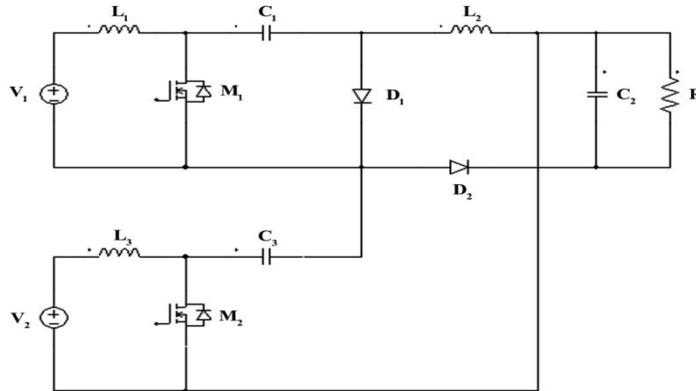


Figure. 2: Circuit diagram of a new hybrid dual input DC-DC converter

### III.MODES OF OPERATION

The operation of the proposed converter can be operating in four modes. Depending on the state of the switches  $M_1$  and  $M_2$  the modes are explained as below.

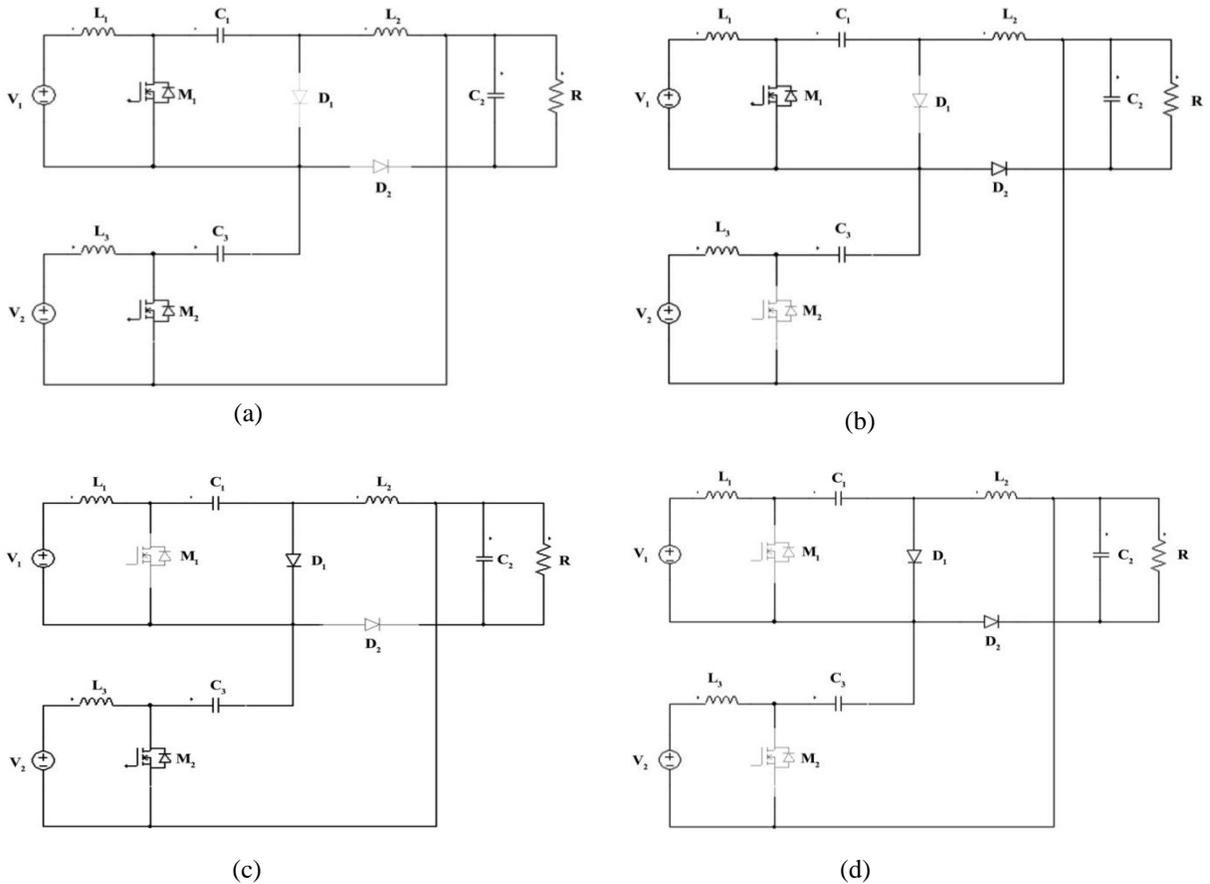


Figure. 3: Equivalent circuit of the proposed converter (a) Mode 1 (b) Mode 2 (c) Mode 3 (d) Mode 4



**Mode 1:** In this mode, the switches  $M_1$  and  $M_2$  are in ON state. By using energy from the sources the inductors  $L_1$  and  $L_3$  becomes charged. The two diodes  $D_1$  and  $D_2$  are not conducting i.e., both diodes are in reverse biased condition. There are three capacitors namely  $C_1$ ,  $C_2$  and  $C_3$  all are in its discharging state. The energy released during the discharging of load capacitor  $C_3$  will be transferred to the load also the inductor  $L_2$  becomes charged. The equivalent circuit of the proposed converter during mode 1 is shown in figure 3(a).

**Mode 2:** In mode 2, the switch  $M_1$  is ON and the switch  $M_2$  is in OFF position. The inductor  $L_1$  continues its state of charging during this mode. But now the inductors  $L_2$  and  $L_3$  release the stored energy in it. Diode  $D_2$  becomes forward biased and starts to conduct by the inductor current  $i_{L3}$ . Diode  $D_1$  remains in the state of reverse biasing. The inductor current  $i_{L3}$  also flows through the load section of the proposed converter. At this time the capacitors  $C_3$  and  $C_2$  becomes charged. Mode 2 equivalent circuit is shown in figure 3 (b).

**Mode 3:** The switch  $M_1$  is in OFF state. The inductor  $L_1$  starts discharging and the inductor current  $i_{L1}$  makes the diode  $D_1$  forward biased and also the capacitor  $C_1$  becomes charged. At the same time the switch  $M_2$  is in ON state and the inductor  $L_3$  becomes charged. Diode  $D_2$  is reverse biased and it will not conduct. As in mode 1, the energy released during the discharging of load capacitor  $C_3$  will be transferred to the load and also the inductor  $L_2$  becomes charged. Figure 3 (c) shows the equivalent circuit of the converter during mode 3.

**Mode 4:**  $M_1$  and  $M_2$  are OFF in this mode. Inductors  $L_1$  and  $L_3$  start to release the stored energy. The diode  $D_1$  and  $D_2$  becomes forward biased by the flow of inductor currents  $i_{L1}$  and  $i_{L3}$ . The output section of the proposed converter is also powered by the inductor current  $i_{L3}$ . Capacitors  $C_1$  and  $C_3$  becomes charged. Also the inductor  $L_2$  releases its energy through diode  $D_1$ ,  $D_2$ , output capacitor  $C_2$  and the load. The equivalent circuit is shown in figure 3 (d).

#### IV.DESIGN CONSIDERATIONS

The input voltage to the Cuk converter i.e., PV array voltage  $V_1$  is taken as 120V. The fuel cell voltage used for the proposed converter is 130V. The switching frequencies of both MOSFETs are of 20KHz.  $D_1$  and  $D_2$  are the duty ratio of switches  $M_1$  and  $M_2$  respectively. Here  $L_1$  is the input inductor and  $C_1$  is the coupling capacitor of Cuk converter section;  $L_3$  is the input inductor and  $C_3$  is the coupling capacitor of Sepic converter section;  $L_2$  is the output inductor;  $C_2$  is the output capacitor;  $R$  is the load resistor. Output voltage,  $V_{out}$  obtained from the converter is 250V and the output power required ( $P_{out}$ ) is 650W.

**Duty ratio:** The duty ratio of the two switches  $M_1$  and  $M_2$  is,

$$D = \frac{V_{out}}{2V_{in} + V_{out}} \quad (1)$$

$$D_1 = \frac{V_{out}}{2V_1 + V_{out}} \quad (2)$$

$$D_2 = \frac{V_{out}}{2V_2 + V_{out}} \quad (3)$$

The value of  $D_1$  is set at 0.51 and  $D_2$  is set at 0.49.

**Load resistor:** The value of the load resistor can be calculated by using the equation

$$R = \frac{V_{out}^2}{P_{out}} \quad (4)$$

The resistance of the load resistor  $R$  is 96.15 $\Omega$ .

**Inductor Selection:**



$$L_1 = V_1 * \left( \frac{D_1}{\Delta I_{L1} * F_{sw}} \right) \quad (5)$$

$$L_2 = (1 - D_1) * \left( \frac{R}{2 * F_{sw}} \right) \quad (6)$$

$$L_3 = V_2 * \left( \frac{D_2}{\Delta I_{L3} * F_{sw}} \right) \quad (7)$$

Where,  $\Delta I_{L1}$  is 30% of input current of Sepic converter section.

$$I_1 = I_{L1} = \frac{P_{in}}{V_1} \quad (8)$$

Where,  $\Delta I_{L3}$  is 30% of input current of Cuk converter section.

$$I_2 = I_{L3} = \frac{P_{in}}{V_2} \quad (9)$$

By substituting these values in (5), (6) & (7); the values of inductors  $L_1$ ,  $L_2$  and  $L_3$  are 1.69 mH, 1.185 mH and 1.91 mH respectively.

#### Capacitor Selection:

$$C_1 = \frac{D_1}{R * F_{sw} * \left( \frac{\Delta V_{C1}}{V_{out}} \right)} \quad (10)$$

$$C_2 = \frac{(1-D_2)}{8 * L_2 * F_{sw}^2 * \left( \frac{\Delta V_{C2}}{V_{out}} \right)} \quad (11)$$

$$C_3 = \frac{D_2}{R * F_{sw} * \left( \frac{\Delta V_{C3}}{V_{out}} \right)} \quad (12)$$

Where,  $\Delta V_{C1}$  is 1% of voltage across the coupling capacitor of Cuk converter section.

$$V_{C1} = \frac{V_1}{(1-D_1)} \quad (13)$$

Where,  $\Delta V_{C2}$  is 1% of voltage across the output capacitor.

$$V_{C2} = \frac{V_2}{(1-D_2)} - V_0 \quad (14)$$

Where,  $\Delta V_{C3}$  is 1% of voltage across the coupling capacitor of Sepic converter section.

$$V_{C3} = \frac{V_2}{(1-D_2)} \quad (15)$$

By substituting these values in (10), (11) & (12); the values of capacitors  $C_1$ ,  $C_2$  and  $C_3$  are 0.268 $\mu$ F, 0.068 $\mu$ F and 0.248  $\mu$ F respectively.



V.SIMULATION RESULTS

The simulation parameters of the proposed converter are given in Table 1. The input voltages  $V_1$  of 120V and  $V_2$  of 130V give an output voltage  $V_{out}$  of 250V for a total output power  $P_{out}$  of 650W.

TABLE 1: SIMULATION PARAMETERS

Parameter	Value
PV Array Voltage, $V_1$	120V
Fuel cell Voltage, $V_2$	130 V
Output Voltage, $V_{out}$	250V
Switching Frequency, $F_{sw}$	20 kHz
Output Power, $P_{out}$	650W
Resistor, R	96.15Ω
Inductor, L1	1.69mH
Inductor, L2	1.185mH
Inductor, L3	1.91mH
Capacitor, C1	0.268μF
Capacitor, C2	0.068μF
Capacitor, C3	0.248μF

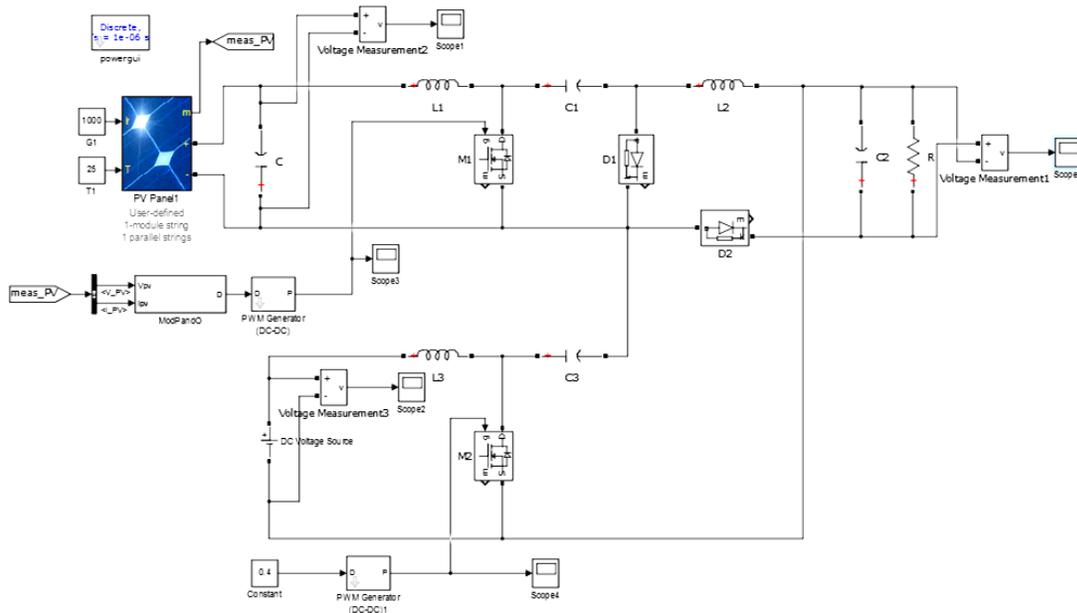


Figure. 4: Simulink model of the proposed converter

The simulink model of the proposed converter is given in figure 4. Simulation results obtained are explained in three sections; simultaneous operation; operation with solar array input only; operation with fuel cell only; as given



below.

**Simultaneous operation:** During simultaneous operation of the proposed converter, the power from both inputs is summed up to deliver power to the load. Input terminal 1 and input terminal 2 are connected to 120V DC and 130V DC respectively during simultaneous operation. The PV array voltage  $V_1$  and fuel cell voltage  $V_2$  are shown in figure 5(a) and figure 5(b). By applying these two input voltages simultaneously, the proposed converter will give an output of voltage 360V and is shown in figure 5(c). Figure 5(d) shows the gate pulses for the MOSFET  $M_1$  and figure 5(e) shows the gate pulses for the MOSFET  $M_2$ . The switching frequencies of both the switches are same with 20 KHz. For the simultaneous operation of the proposed converter, pulses have to be given to both switches  $M_1$  and  $M_2$ .

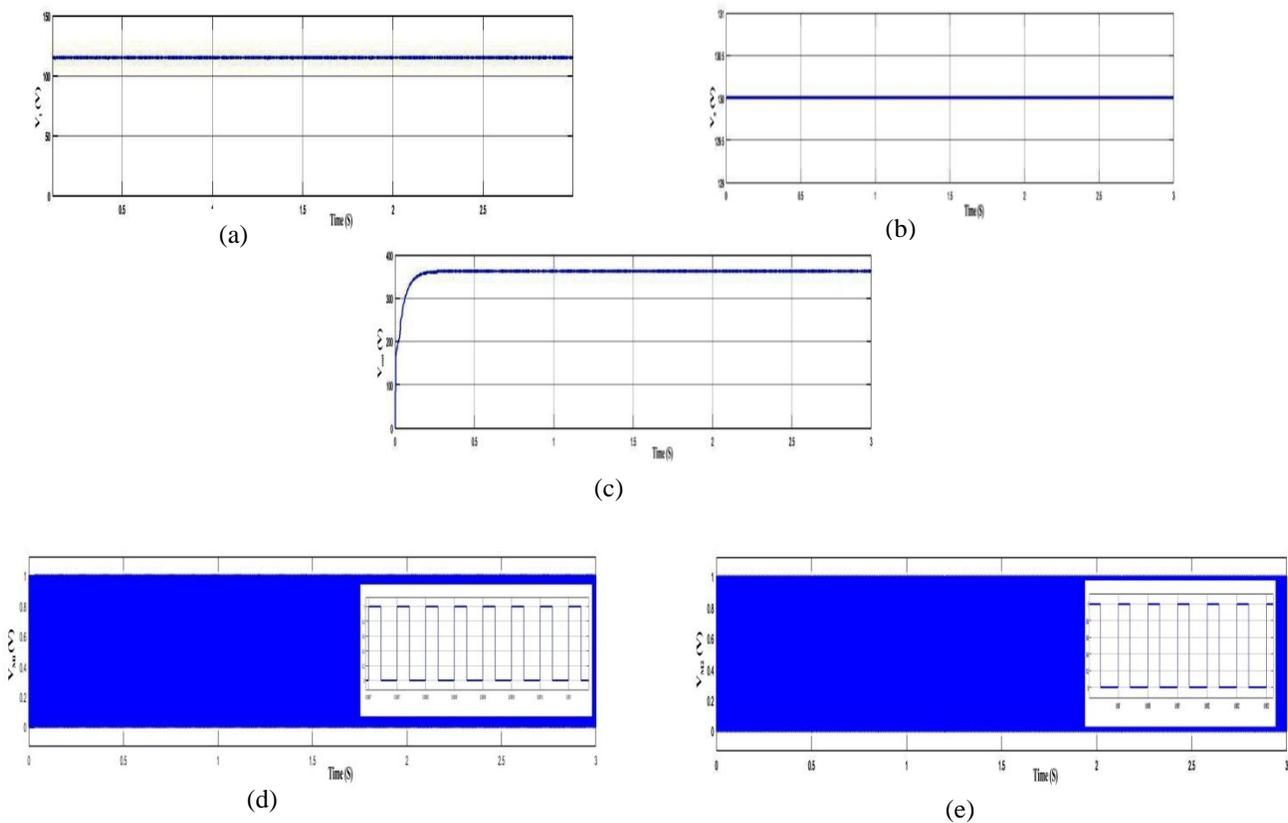


Figure. 5: (a) PV array voltage  $V_1$  (b) Fuel cell voltage  $V_2$  (c) Output Voltage (d) Gate pulses for  $M_1$  (e) Gate pulses for  $M_2$

**Operation with solar array input only:** During individual operation, one of the input sources to the converter is unavailable and it has to continue its operation with the remaining input source. In this case, there is only solar array input is present. Now the fuel cell voltage  $V_2$  is 0V. Figure 6(a) shows the PV array voltage  $V_1$  and figure 6(b) shows the gating pulses applied to the switch  $M_1$ . The output voltage of the proposed converter with solar array input only is shown in figure 6(c).

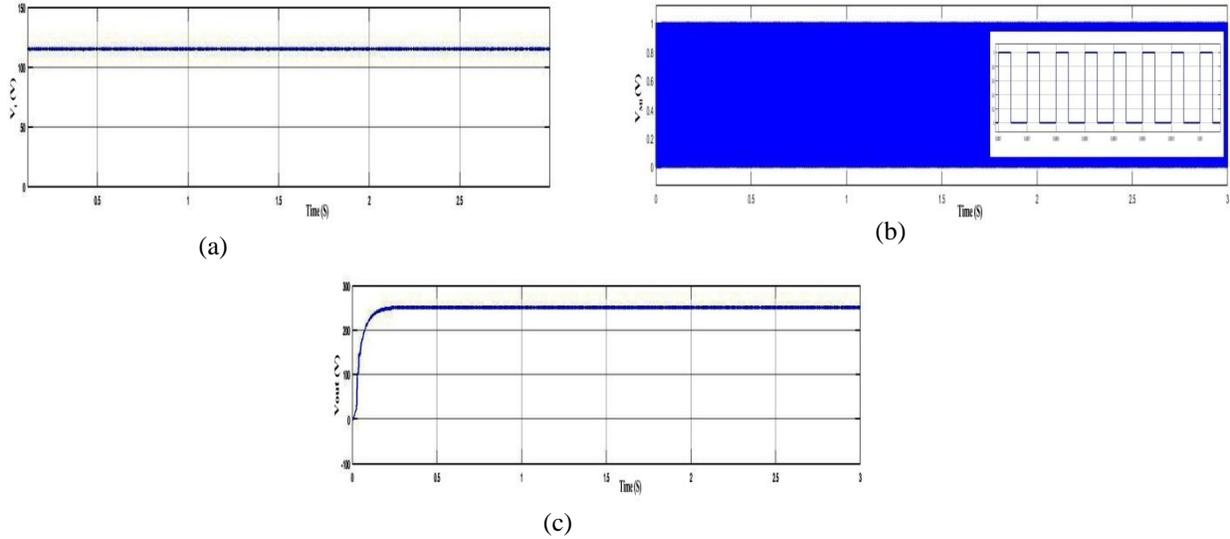


Figure. 6: (a) PV array voltage  $V_1$  (b) Gate pulses for  $M_1$  (c) Output Voltage

**Operation with fuel cell input only:** In this case, there is only fuel cell input is present. Now the PV array voltage  $V_1$  is 0V. Figure 7(a) shows the fuel cell voltage  $V_2$  and figure 7(b) shows the gating pulses applied to the switch  $M_2$ . The output voltage of the proposed converter with solar array input only is shown in figure 7(c).

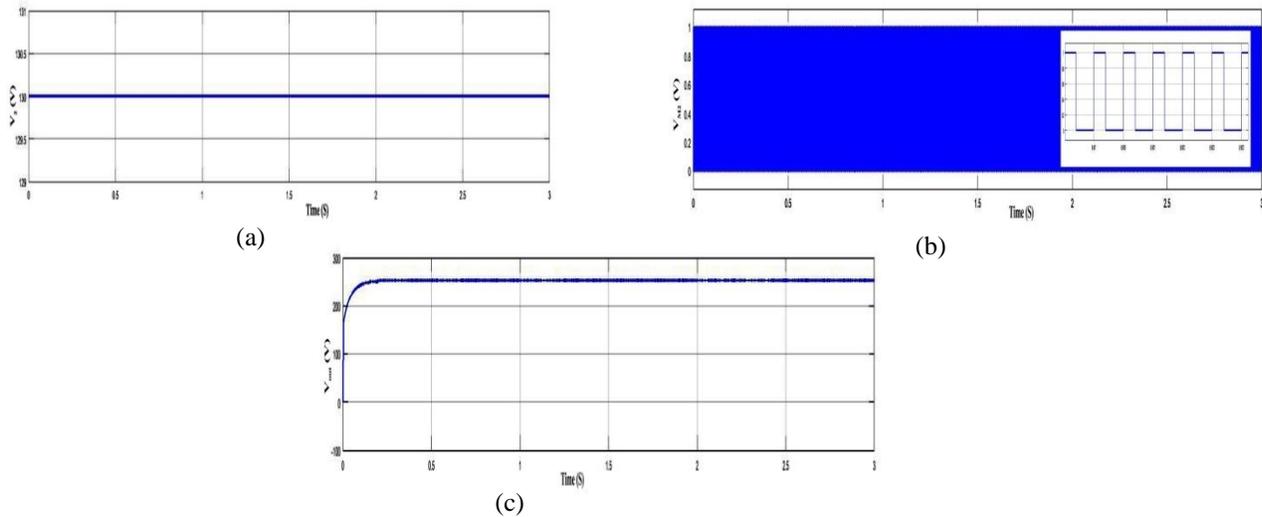


Figure. 7: (a) Fuel cell voltage  $V_2$  (b) Gate pulses for  $M_2$  (c) Output voltage

If the availability of the sunlight is decreased due to worst climatic conditions or during night time, the fuel cell can compensate the output voltage. To explain the proposed converter topology considering that, in the presence of better solar radiation the irradiance is about  $1000\text{W/m}^2$ . For example, if the irradiance is low about  $500\text{W/m}^2$  the output of the proposed converter without fuel cell is also low with a value 200V as shown in figure 8(a). But proposed converter is capable of producing the output voltage of 250V with the presence of fuel cell. Figure 8(b) shows the output voltage of proposed converter with fuel cell during low solar radiation.

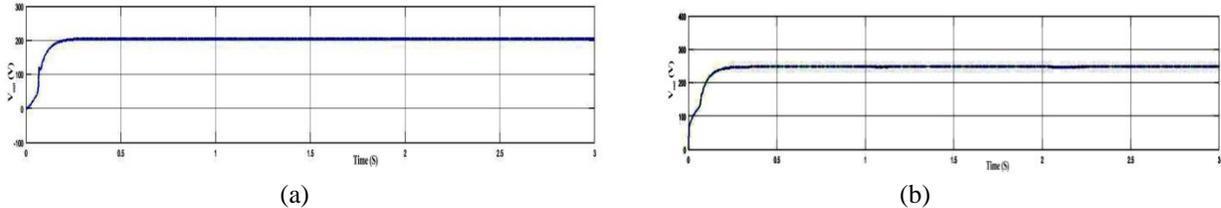


Figure. 8: (a) Output voltage of the proposed converter without fuel cell at irradiance 500W/m<sup>2</sup> (b) Output voltage of the proposed converter with fuel cell at irradiance 500W/m<sup>2</sup>

### VI. ANALYSIS

The analysis of a new hybrid dual input DC–DC converter is carried out by considering the parameters output voltage and irradiance. Typical curves for the variation of output voltage as a function of irradiance with fuel cell and without fuel cell are shown in figure 9(a) and figure 9(b). From these figures we can say that the output voltage of the proposed converter is maintained at 250V even when solar irradiance is low due to worst climatic condition or during night time.

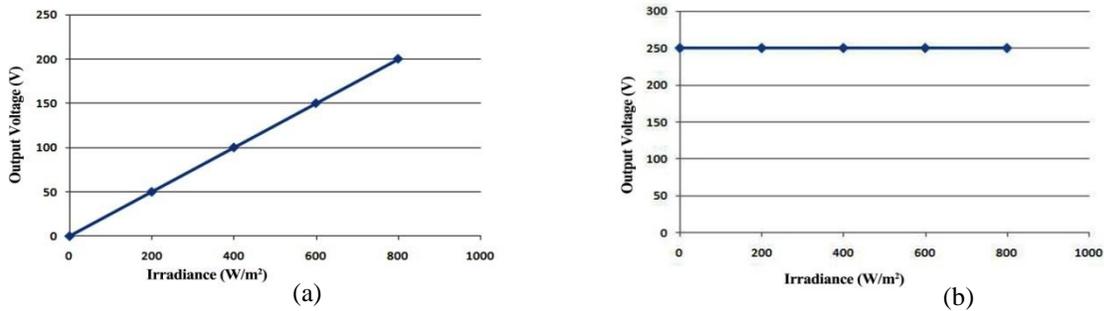


Figure. 9: (a) Output voltage Vs Irradiance (Without fuel cell) (b) Output voltage Vs Irradiance (With fuel cell)

### VII. CONCLUSION

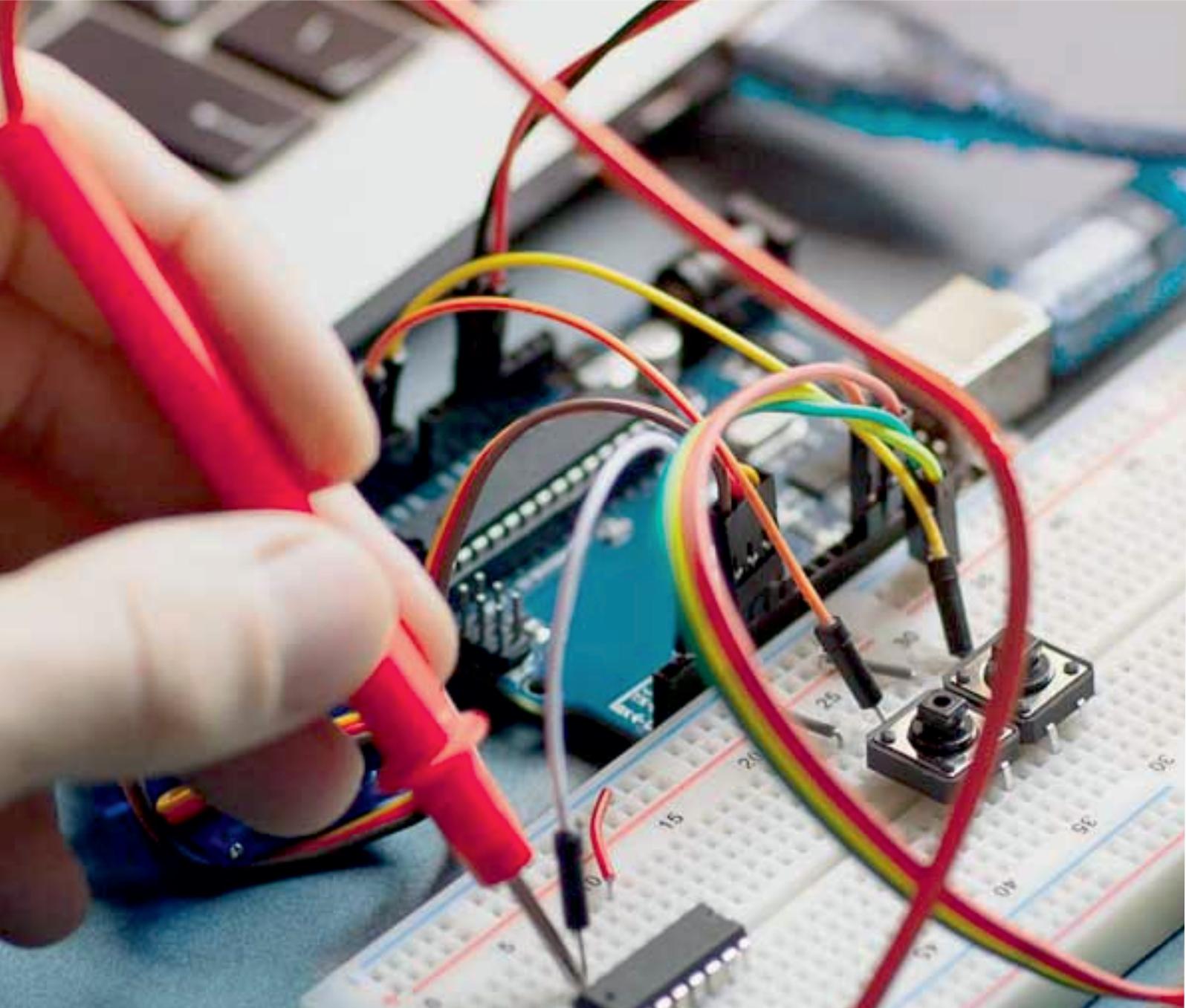
This paper proposes a new hybrid dual input DC-DC Converter with P&O algorithm employing MPPT for renewable energy applications. The proposed converter is a combination of Sepic converter and Cuk converter. By combining these two converters can be eliminate separate input filters. If the availability of the sunlight is decreased due to worst climatic condition or during night time, the fuel cell can compensate the output voltage. So a constant output voltage is always maintained to meet the energy demand. The circuit also have an advantage of individual and simultaneous operation. By using a renewable energy as the main input the operating cost can be minimized. This system finds applications in remote area power generation, constant speed energy conversion systems, variable speed energy conversion systems, rural electrification, water pumping system, etc...

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