PID Controller Based Automatic Reactive Power Control of a Wind-Diesel Hybrid Power System

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ABSTRACT: The study investigates the application of PID controller approach to stabilise the reactive power control of a Hybrid wind-diesel system. The above system consists of a synchronous generator for diesel generator, Induction generator for wind system, a STATIC VAR COMPENSATOR and Automatic voltage regulator for stabilizing of load terminal Bus. Here by controlling the firing angle SVC and gains of PID controller the voltage profile at load terminal is got improved. The performance of the Hybrid system with PID controller and without PID controller is investigated by MATLAB simulation software.

KEYWORDS: Induction generator, synchronous generator, static var compensator, Thyristor Controlled Reactor

I. INTRODUCTION

The need of power is continuously increasing day by day. The conventional fossil fuel power is unable to mitigate the the demand in today’s date. Therefore today’s technology wants a power delivered to be reliable and should be eco-friendly in nature. There by renewable sources is found to be more efficient. One of them is wind-diesel Hybrid power system. [1-3]. The advantage of Hybrid power is that it continuously uses power generation as well as non-polluting wind energy. In hybrid power generation there can be more than one electrical generation. Basically Synchronous generator is used for diesel power and Induction Generator is used for wind power. Induction generator have advantage over synchronous generator as it is less in cost, less maintenance, rugged etc. but again its main disadvantage is that it needs reactive power for operation. Now with the increasing amount of non-linear Load the power quality issue has made the power system unstable. The power quality issue include voltage flicker, maintain reactive power, Harmonics etc. Although different power quality equipment i.e like Active power filter, static synchronous compensator have been used [4-6] but due to their high cost its use has been limited. In order to mitigate cost issue static var compensator(SVC) which uses thyristor phase controlled technology still a cost-effective solution to mitigate power quality issue[7-8].

In this paper a standalone hybrid power system is taken for a case study. During adverse condition voltage may decreases or increases in order to overcome voltage instability a PID based automatic reactive controller is designed with SVC which will helps to improve the voltage profile. The system state equation has been obtained as different block Diagrams. The Voltage deviation error has been used to eliminate reactive power insufficiency of the plant. The mathematical model of the Hybrid is shown in the section 2. This Hybrid model model is simulated using matlab Simulink environment. At Last comparison of result between this Hybrid-wind diesel model with SVC without PID controller and with PID controller is shown in section.

II. SVC SYSTEM CONFIGURATION

A. SVC configuration:- Providing shunt compensation in transmission line using shunt capacitors bank is an obsolete technology. Because neither it can provide sudden compensation during overload condition nor it can provide stability
during contingency condition. This shunt capacitor may look inexpensive but it lacks dynamic compensation. We know that the phase angle between the two end voltage which is determined by real component line current is independent of shunt compensation. So we can add a reactor instead of capacitor to decrease the voltage in transmission line[8]. Instead of using any devices like circuit breaker we can use thyristor valve to increase voltage control more efficiently. This is method is known as static varcompensator(SVC). The basic reactive component of SVC is a shunt reactor and shunt capacitor. The reactors are varied by using thyristor switching.

B. Basic description of static varcompensator(SVC):- SVC can be one of the following type

1. Thyristor Controlled Reactor(TCR)
2. TCR plus Fixed Capacitor(FC)
3. Thyristor Switched Capacitor(TSC)
4. TSC plus TCR

The fourth one is very popularly used. Fig.1 shows an one line diagram of SVC in transmission line. The idea is to sense voltage of the line and make the line stable by injecting inductance or capacitance depending on the signal generated by circuit by Automatic Voltage Regulator(AVR). So the gating signal will depend on the AVR signal. By controlling the conduction time of thyristor we can control voltage in each cycle. That’s why this type of control is very fast and accurate.

![Fig1. Typical SVS system](image)

C. Reactive power compensation through SVC:- The two function of svc is to absorb or to generate reactive power. Generally thyristor switched capacitor(TSC) are used for absorb of reactive power where as Thyristor controlled reactor(TCR) for generation of reactive power purpose TSC provides harmonics free control whereas TCR gives continuous control of reactive power with SVC we can provide a good voltage profile with sufficient speed of response under transient condition. Now a days the SVC system is applied in all transmission system developments.

III. MATHEMATICAL MODEL OF WIND-DIESEL SYSTEM

In Fig 3 a wind diesel system is shown which is considered for mathematical modelling. The following model consists of a synchronous generator(SG) which is a IEEE type3 excitation system connected with DG and a Induction generator(IG) which is driven by wind turbine. In the following model a SVC is connected to provide the required reactive power in addition to in addition to reactive power generated SG. Small changes in active power reflect as a change of frequency where as small change in reactive power reflects as a change of reactive power.[9]
The excitation time constant is smaller than prime mover time constant and its transient decay is much faster. The reactive balance equation at steady state is

\[ \Delta Q_{SVC} + \Delta Q_{SG} = \Delta Q_{IG} + \Delta Q_L \]  

(1)

Where Assuming the change in load reactive power is equal to \( \Delta Q_L \)

Due to load the system reactive power increases by the amount \( \Delta Q_{SVC} + \Delta Q_{SG} \)

The net reactive power can be written as

\[ \Delta Q_{net} = \Delta Q_{SVC} + \Delta Q_{SG} - \Delta Q_{IG} - \Delta Q_L \]  

(2)

This power will increases the terminal voltage in two ways.

1) It increases the electromagnetic absorption (Em) of the induction generator (IG) at rated \( d/dt (Em) \).

2) It increases the reactive load consumption of the system.

This can be represent mathematically as

\[ \Delta Q_{SG} + \Delta Q_{SVC} - \Delta Q_L - \Delta Q_{IG} = d/dt (\Delta EM) + D_\psi \Delta V \]  

(3)

The electromagnetic energy stored in IG is given by

\[ E_M = \frac{1}{2} L_M I_M^2 = \frac{V_t^2}{4\pi f X_M} \]  

(4)

Where, \( I_M, L_M, \) and \( X_M \) represents the current, inductance, and reactance of the Induction Generator respectively. Here \( f = \) system frequency

From eqr(4), \( \Delta EM \) can be written as

\[ \Delta E_M = E_M - E_M^0 = 2 (E_M^0 V_t^0) \Delta V_t \]  

(5)

where \( E_M^0 \) and \( V_t^0 \) represents nominal value of electromagnetic energy stored IG and terminal voltage.

When the voltage increase all connected reactive power loads increased by \( D_\psi = \frac{\partial Q_L}{\partial V_t} \) (per unit kilovolts)

The reactive power load can be expressed as [10] \( Q_L = C_1 V_q \)  

(6)

Where \( C_1 \) is the constant of the load and the exponent depends on the type of the load.

For a small perturbation load and voltage characteristics represented as

\[ \Delta Q_L/\Delta V_t = q (Q_L^0/V_t^0) \]  

(7)

Where \( Q_L^0 \) is the load reactive power

Using eqr(5) and eqr(3) we get
ΔQ_{SG} + ΔQ_{SVC} − ΔQ_{L} − ΔQ_{IG} = 2E'M/(V'tQ_r) d/dt (ΔV_r) + DvΔV_r.....(8)

Where Q_r is the system power rating. The term E'M/Q_r can also be written as
E'M/Q_r = 1/(4πf_k) = H_r ........................................(9)

Where the term k_r refers the ratio of the system reactive-power rating to rated magnetizing reactive power of IG. Substituting in Eq(9) in (8) we will get

ΔQ_{SG} + ΔQ_{SVC} − ΔQ_{L} − ΔQ_{IG} = 2H_r/V't^2 d/dt (ΔV) + DvΔV_r....(10)

Taking Laplace Transform Both sides

ΔV_r(s) = KV / (1 + sT_v) × [ΔQ_{SG}(s) + ΔQ_{SVC}(s) − ΔQ_{L}(s) − ΔQ_{IG}(s)].....(11)

The complete block diagram of above mathematical equation is shown in fig.3

Fig 3 complete block diagram of hybrid diesel-wind system

Where \( \frac{2H_r}{DvVo} \cdot K_v = \frac{1}{dv} \) Under transient condition \( Q_{SG} = (E_qV \cos \delta − V^2)/X_D \) ........................................(12)

For small perturbation, (12) can be written as \( ΔQ_{SG} = (V \cos \delta/X_D) ΔE_q + [(E_q \cos \delta - 2V)/X_D] ΔV_r .....(13) \)

In Laplace transform, (13) can be written as \( ΔQ_{SG}(s) = K_3ΔE_q(s) + K_4ΔV (s) \) .........................(14)

Where \( K_3 = (V \cos \delta/X_D) \) And \( K_4 = E_q \cos \delta - 2V/X_D \) .................................................(15)

The reactive power supplied by the SVC is given by:-

\( Q_{SVC} = V^2 B_{SVC} \) .................................................................(16)
For small perturbation, (19) in the Laplace-transform form can be written as:

\[ \Delta Q_{\text{svc}}(s) = K_6 \Delta V(s) + K_7 \Delta B_{\text{svc}}(s) \]  

(17)

Where \( K_6 = 2B_{\text{svc}} \). The flux linkage equation [12] of the round rotor synchronous machine for small perturbation is given as

\[
\frac{d}{dt} (\Delta E_q) = \frac{\Delta E_{fd} - \Delta E_q}{T_d} \]  

(18)

In (17), \( \Delta E_q \) is given by

\[
\Delta E_q = \frac{X_d}{X_d'} \Delta E_q'' - X_d - X_d' \cos \delta \Delta V \]  

(19)

For small changes, (18), using (17) in the Laplace-transform form, can be written as:

\[
(1 + sT_G) \Delta E_q = K_1 \Delta E_{fd}(s) + K_2 \Delta V(s) \]  

(20)

Where \( T_G = \frac{X_d T_{do}}{X_d} \)  

(21)

\[
K_1 = \frac{X_d}{X_d'} \]  

(22)

\[
K_2 = \frac{(X_d - X_D) \cos \delta}{X_d} \]  

(23)

for small perturbation, reactive power absorbed by IG, \( Q_{\text{IG}} \) in terms of generator terminal voltage, and generator parameters can be written as

\[
\Delta Q_{\text{IG}} = K_5 \Delta V(s) \]  

(24)

Where \( K_5 = \frac{2V_{\text{eq}}R_y}{X_{\text{eq}}^2} \)  

(25)

\[
R_p = R_y - R_{eq} \]  

(26)

Then the state space model of reactive power control of the hybrid wind-diesel

\[
\dot{X} = Ax + Bu + Ed \]  

Where \( A = [\Delta E_{fd} \Delta V_I \Delta V_{er} \Delta E_q \Delta B_{svc} \Delta V_I] \)  

\( U = [\Delta V_{er}] \)  

\( d = [\Delta Q_I] \)

IV. WIND-DIESEL SYSTEM DATA

In order to execute our Hybrid wind-diesel system we have taken some reference parameters such as Diesel capacity, wind capacity, Load capacity etc. which is listed below in Table.1. The optimum gain setting of PID parameters is also listed in this table.

<table>
<thead>
<tr>
<th>Table.1 System parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Diesel capacity</strong></td>
</tr>
<tr>
<td><strong>Wind capacity</strong></td>
</tr>
<tr>
<td><strong>Load capacity</strong></td>
</tr>
<tr>
<td><strong>Synchronous Generator</strong></td>
</tr>
<tr>
<td>( P_{\text{sc}} ) (pu Kw)</td>
</tr>
<tr>
<td>( Q_{\text{sc}} ) (pu KVAR)</td>
</tr>
<tr>
<td>( E_p ),pu</td>
</tr>
<tr>
<td>( \delta )</td>
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<tr>
<td><strong>Induction Generator</strong></td>
</tr>
<tr>
<td>( P_{\text{ig}} ) (pu Kw)</td>
</tr>
<tr>
<td>( Q_{\text{ig}} ) (pu KVAR)</td>
</tr>
<tr>
<td>( S )</td>
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<tr>
<td>( r1,r2 ) in pu</td>
</tr>
</tbody>
</table>
V. RESULTS AND DISCUSSION

Simulation results of above system is shown in fig.6, fig.7 and in fig.8. The effectiveness of proposed scheme is done through a step change in load reactive power.

A. Comparison of terminal voltage with and without PID controller. The effectiveness of using PID results in improvement of voltage at load side can be seen from the results.

B. Reactive power of I.G: In fig 7 the reactive power of I.G is shown with same PID and without PID controller. The improvement of reactive power of I.G can be seen at load side. The damping is reduced after 3sec.

### Table: Load and Gain of PID controller

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Load</td>
<td></td>
</tr>
<tr>
<td>P(Pu Kw)</td>
<td>1</td>
</tr>
<tr>
<td>Q(pu KVAR)</td>
<td>.75</td>
</tr>
<tr>
<td>PF lag</td>
<td>.8</td>
</tr>
<tr>
<td>Gain of PID controller</td>
<td>35,5238, 35</td>
</tr>
<tr>
<td>Kp, Ki, Kd</td>
<td></td>
</tr>
</tbody>
</table>
VI. CONCLUSION

This paper investigates the improvement of voltage profile of a Hybrid wind diesel renewable set via considering a transfer function model approach. This model consists of a Synchronous generator driven by diesel engine and an induction generator driven by wind turbine and a thyristor-controlled Staticvar compensator. The state space equation was developed for the above model. It was shown that this model needs reactive power to improve its voltage profile. For the above purpose a PID controller is incorporated. The reactive power at load side is tested using step change of load reactive power. Finally by simulation results it was shown that by using the above controller not only we mitigate reactive power deficiency but also the damping is reduced.

REFERENCES