



# **A Novel ZVS Step up Converter for Renewable Energy Generation Applications**

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**ABSTRACT:** This paper introduces a novel ZVS step up converter especially for renewable energy generation applications. The proposed converter is consisting of single switch which operates in zero voltage and zero current. Resonant principles are opted for soft switching. High voltage gain is obtained by switched capacitor cell topology. Use of single switch will reduce the cost of conversion and complexity of control circuits. The circuit topology consisting of resonant inverter with zero voltage switching with an energy blocking diode having zero current switching. The energy blocking diode with DC output filter filters the output stage of converter.

**KEYWORDS:** Switched capacitor, Resonant power converter, zero-current switching, zero-voltage switching, pulsewidth modulation

## **I. INTRODUCTION**

Now a days, global surface temperatures have increased drastically, because the global warming is taking place due to effluent gas emissions and increases in Carbon Monoxide. To prevent these effects, some potential solutions have evolved including energy conservation through improved energy efficiency, a reduction in fossil fuel use and an increase in environmental friendly energy sources. However, the output voltage of these sources is too low and which requires a voltage boost. In this stage, efficiency of conversion is a major concern. Efficiency in the sense minimizing the switching and conduction losses.

## **II. LITERATURE SURVEY**

In transformer isolated dc-dc converters, by increasing the turns ratio, we can boost the voltage gain. But, when we increase the turns ratio, leakage inductance will also increase, which will lead to high voltage stress and poor efficiency [1]. In case of non-isolated dc-dc converter topologies, boost converter is using for voltage boost up. But duty cycle limitation is the problem associated. As duty cycle increases, inductor current ripple and turn off current of the power device will increase, which leads to large conduction loss and degraded efficiency [2]. Cascaded boost converters can increase the voltage gain, however component count will increase hence size and cost of converter also [3]. Integrating coupled inductor into the non-isolated dc-dc converter by choosing a suitable turns ratio can increase the voltage gain effectively. In order to absorb the energy stored in leakage inductor, a snubber circuitry is needed which will increase circuit complexity and loss of efficiency [4]. Switched capacitor cell converters can obtain a very high voltage gain, however input current pulsation is a problem and poor load and line voltage regulation. Incorporating switched capacitor structure into switching mode dc-dc converter is a good remedy for this problems. Hence we can dramatically increase voltage gain with an appropriate duty cycle with good voltage regulation and minimum input current pulsation [5].

Pulse width modulation is the simplest method for controlling power semiconductor switches. PWM power converters can now operate at a much higher switching frequency hence reducing the size of passive components and the overall cost of the system. But, the converter switching loss also increases in proportion to the frequency. As switching frequency increases time derivative of voltage and current will also increase which will lead to increased stress on the device. To solve this problem, some soft-switching approaches must be used at high switching frequencies. Resonant converters can solve these high voltage and current stress problems and ensuring both high performance and supporting energy conservation applications in renewable energy generation systems. Two commonly used soft-switching

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 8, August 2015

methods are Zero voltage switching and zero-current switching i.e., either voltage or current is zero during the switching transition, substantially reducing the switching loss and increasing the reliability of resonant converters in renewable energy generation systems [6].

This work introduces a novel single-switch high step up converter with ZVS topology based on the traditional ZVS concept for renewable energy generation applications. Voltage step up is by adopting the principals of switched capacitor cell topology. The main features of this converter is that single switch operation, simple circuit, soft switching, ease of control, low switching losses and high voltage boost up. This circuit utilizes a capacitor across the active power switch to generate a freewheeling stage with a traditional ZVS power converter, enabling the novel converter to operate with a constant frequency and a markedly much reduced circulating energy. Main operating principal of switched capacitor cell is that, capacitor cells charges in parallel and discharges in series. As the number of capacitor cells increases, the output voltage will also increase. In this converter we are using single capacitor cell. This paper shows the operational analysis and simulation results of the proposed converter.

### III. CIRCUIT DESCRIPTION

This work integrates a novel current-fed resonant converter with switched capacitor cell topology in order to increase the voltage level. Resonant converter with ZVS and ZCS operations of both the active power switch and the rectifying diode for energy conversion. Fig.1 shows a basic circuit diagram of the proposed novel ZVS and ZCS single-switch step up converter for renewable energy generation applications.

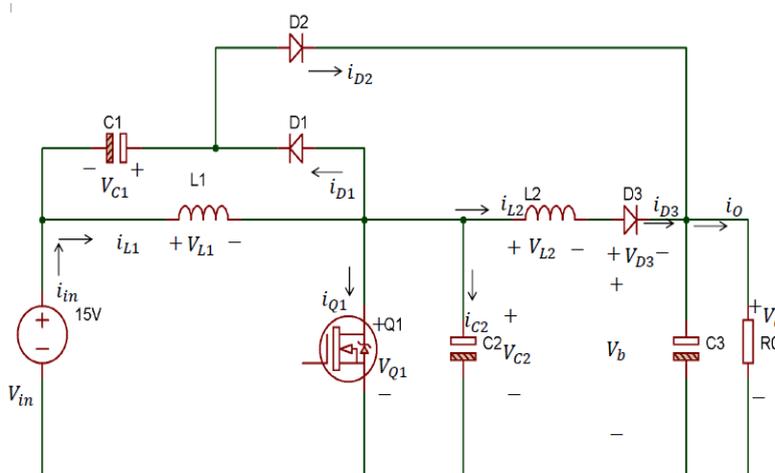


Fig. 1 Proposed circuit

The circuit consisting of a choke inductor  $L_1$ , a metal-oxide-semiconductor field-effect transistor (MOSFET) that operates as a power switch  $Q_1$ , The capacitor  $C_1$  is connected in series to source voltage and load resistor through diode  $D_2$ , a shunt capacitor  $C_2$ , a resonant inductor  $L_2$ , an energy-blocking diode  $D_3$ , and a filter capacitor  $C_3$ . The capacitor  $C_3$  and the load resistance  $R_0$  together form a first-order low-pass output filter, which reduces the ripple voltage below a specified level. The MOSFET is the favoured device because its body diode can be used as an antiparallel diode  $D_E$ , for a bidirectional power switch. Notably, the shunt capacitance  $C_2$ , includes the power switch parasitic capacitance and any other stray capacitances (such as the winding capacitance of the choke  $L_1$ ). Careful design of the circuit parameters guarantees that the power switch  $Q_1$  is switched by ZVS and the energy-blocking diode  $D$  is switched by ZCS, optimizing the operation of the converter.

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 8, August 2015

## IV. PRINCIPLE OF OPERATION

The novel ZVS single-switch step up converter for renewable energy generation applications is analysed using the following assumptions.

- The switching elements of the converter are ideal, such that the drop in forward voltage across the resistance of the power switch in the ON state is negligible.
- The equivalent series resistance of the capacitance and stray capacitances is negligible.
- The characteristics of the passive components are linear, time invariant, and independent of frequency.
- The filter capacitance  $C_3$  at the output terminal is typically very large; the output voltage across capacitor  $C_3$  can therefore be treated as an ideal dc voltage in each switching cycle.

The key waveforms for each mode of the proposed converter are shown in Fig. 2. One switching cycle is divided into six modes, which are described as follows.

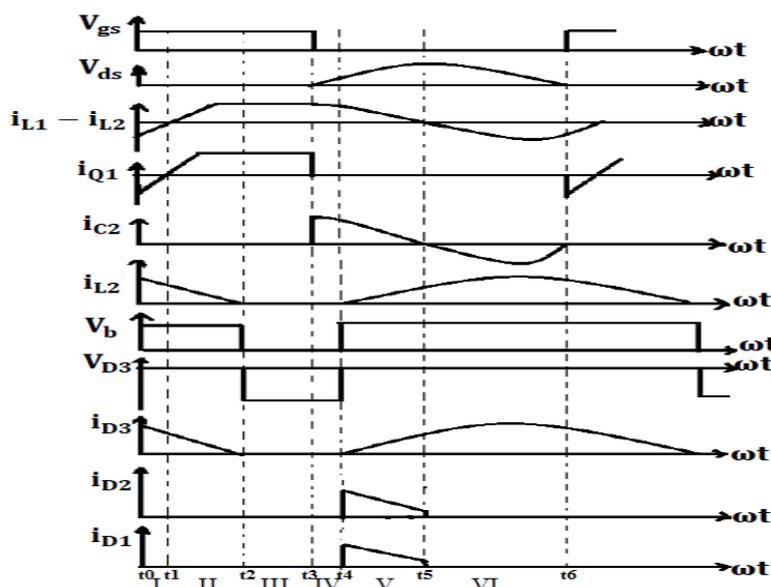


Fig. 2 Switching waveforms

Mode 1 —Between  $t_0$  and  $t_1$ : Prior to Mode 1 operation, power switch  $Q_1$  is off. The resonant tank current  $i_{L2}$  is positive and higher than the dc input current  $i_{L1}$ . The switch must be turned on only at zero voltage. Otherwise, the energy stored in the capacitor  $C_2$  will be dissipated in the active power switch  $Q_1$ . To prevent this situation, the antiparallel diode  $D_E$  must conduct before the power switch is turned on. Since the capacitor current  $i_{C2}$  is negative, it flows through capacitor  $C_2$ . When the capacitor voltage  $V_{C2}$  falls to zero, a turn-on signal is applied to the gate of the active power switch  $Q_1$ . Therefore, the active power switch  $Q_1$  turns on under ZCS and ZVS conditions. At the beginning of this mode, since the difference between currents  $i_{L1} - i_{L2}$  is negative, the antiparallel diode  $D_E$  conducts. The energy-blocking diode  $D_3$  is turned on because the resonant tank current  $i_{L2}$  is positive. Diodes  $D_1$  and  $D_2$  are reverse biased. Fig. 3 represents the equivalent circuit of this mode. Mode 1 ends as soon as the antiparallel diode  $D_E$  is reverse biased by a positive current  $i_{L1} - i_{L2}$ .

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 8, August 2015

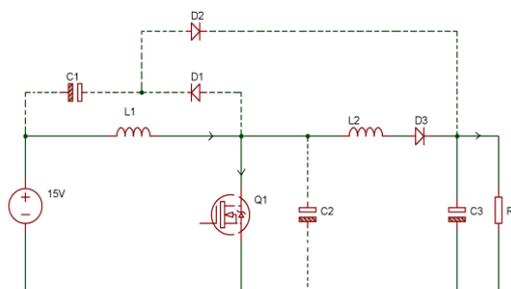


Fig. 3 Mode 1 Operation

Mode 2 —Between  $t_1$  and  $t_2$ : In this mode, the active power switch  $Q_1$  remains in the ON state. Fig. 4 shows the equivalent circuit. The input line voltage is applied to the choke inductor  $L_1$ , and  $i_{L1}$  increases continuously. In this mode, the current  $i_{L1} - i_{L2}$  commutates the antiparallel diode  $D_E$  and turn on active power switch  $Q_1$ . Hence, the voltage across the capacitor  $C_2$  is clamped at zero. The resonant current  $i_{L2}$  passes through the energy-blocking diode  $D_3$ . The circuit operation enters Mode 3 when the inductor current  $i_{L2}$  falls to zero.

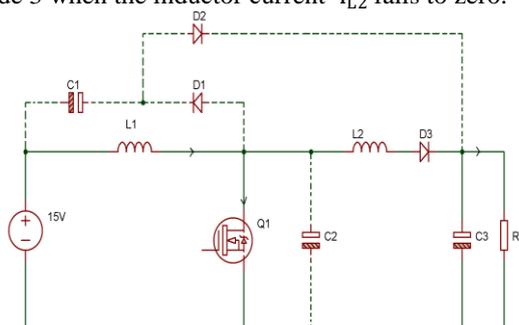


Fig. 4 Mode 2 Operation

Mode 3 —Between  $t_2$  and  $t_3$ : In this mode, the switch  $Q_1$  remains in the ON state, and the input dc current  $i_{L1}$  continuously rises. The input inductor current  $i_{L1}$  flows through the power switch  $Q_1$ . The resonant inductor current  $i_{L2}$  falls until it reaches zero and is prevented from going negative by the energy-blocking diode  $D_3$ . Energy is stored in the choke inductor  $L_1$  when the active power switch is turned on and is transferred to the output load when the active power switch is turned off. Fig. 5 displays the equivalent circuit of this mode. Mode 3 is exited at the time when the power switch  $Q_1$  is turned off.

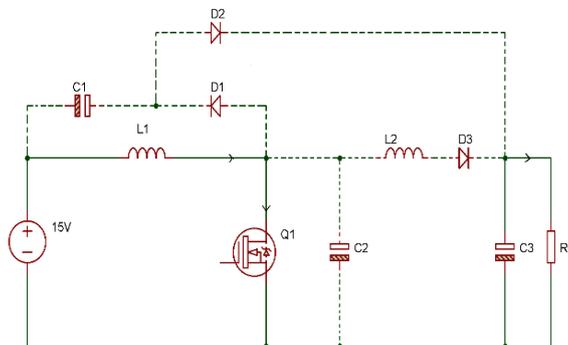


Fig. 5 Mode 3 Operation

Mode 4 —Between  $t_3$  and  $t_4$ : At the beginning of this mode, switch  $Q_1$  is switched off. The resonant capacitor current  $i_{C2}$  becomes  $i_{L1}$ . Then, the capacitor voltage  $v_{C2}$  rises from zero to a finite positive value. For ZVS operation,  $Q_1$  is switched off at zero voltage, and the capacitor voltage  $v_{C2}$  increases linearly from zero at a rate that is proportional to input inductor current  $i_{L1}$ . The capacitor current  $i_{C2}$  flows through capacitor  $C_2$  to charge  $C_2$ , transferring the energy

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 8, August 2015

from the dc input source to capacitor  $C_2$ . During this mode, the output power of load resistor  $R_0$  is supplied by the output capacitor  $C_3$ . Fig.2 reveals that the active power switch  $Q_1$  is turned off under the ZVS condition. Fig.6 presents the equivalent circuit. Mode 4 ends when the energy-blocking diode  $D_3$  is forward biased ( $v_{C2} > V_0$ ). Then, the circuit operation enters next mode.

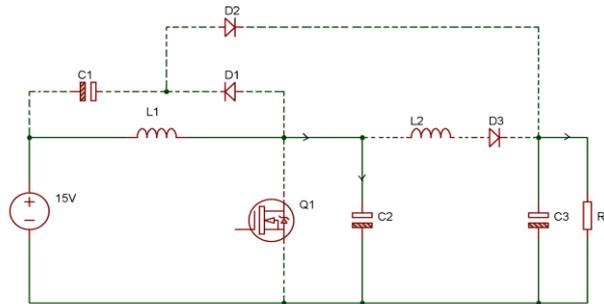


Fig. 6 Mode 4 Operation

Mode 5 —Between  $t_4$  and  $t_5$ : In this mode, the active power switch  $Q_1$  remains in the OFF state. The resonant inductor current  $i_{L2}$  is positive, and the energy-blocking diode  $D_3$  is turned on, yielding a resonant stage between inductor  $L_2$  and capacitor  $C_2$ . In this time, the capacitor current  $i_{C2}$  is still positive. Hence, the capacitor voltage  $v_C$  continues to increase to its peak value. Diodes  $D_1$  and  $D_2$  in the conducting state. The capacitor  $C_1$  discharges its energy to the load via diode  $D_2$ . Fig. 7 presents the equivalent circuit. Mode 5 ends when capacitor current  $i_{C2}$  resonates to zero at  $t_5$ , and next operating begins.

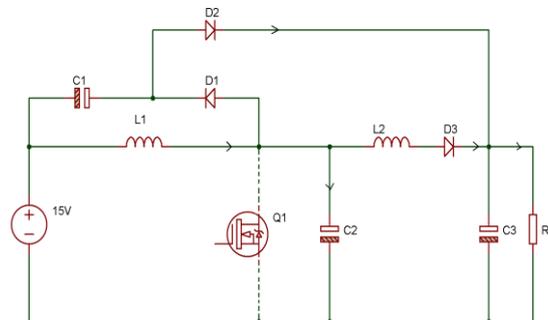


Fig. 7 Mode 5 Operation

Mode 6 —Between  $t_5$  and  $2\pi$ : This mode begins at  $t_5$  when capacitor voltage  $v_{C2}$  resonates from negative values to zero. The active power switch  $Q_1$  is turned on when  $\omega t = 2\pi$  to eliminate switching losses. Fig. 8 illustrates the equivalent circuit.

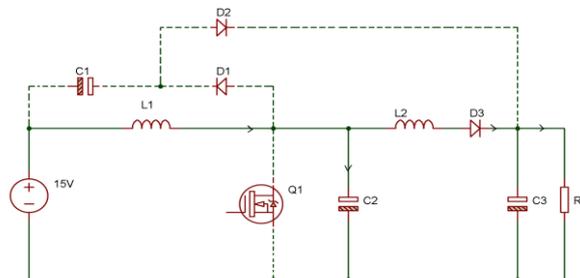


Fig. 8 Mode 6 Operation

Before the cycle of the resonant inductor current  $i_{L2}$  oscillation ends, the active power switch  $Q_1$  is kept off condition, constraining the positive current to flow continuously through the energy-blocking diode  $D_3$ . In addition to the active power switch, the energy-blocking diode in the novel converter is also commutated under soft switching. When the

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 8, August 2015

driving signal  $V_{gs}$  again excites the active power switch  $Q_1$ , this mode ends, and the operation returns to Mode I in the following cycle.

## V.SIMULINK MODEL

To verify the feasibility and validity of the proposed converter, MATLAB/Simulink software is applied for the simulation of the converter. The input of the proposed novel ZVS single-switch step up power converter can be connected to a small-scaled solar energy generation system that consisting of a dc source with an output voltage of 15 V. Fig. 9 shows the Simulink model of the proposed converter. The following parameters are used in this simulation model. DC input voltage of 15V.  $L_1 = 25\mu\text{H}$ ,  $L_2 = 19\mu\text{H}$ ,  $C_1 = 0.82\mu\text{F}$ ,  $C_2 = 0.1\mu\text{F}$ ,  $C_3 = 220\mu\text{F}$ ,  $P_0 = 16\text{W}$ ,  $V_0 = 55\text{V}$ ,  $f_s = 70\text{kHz}$ .

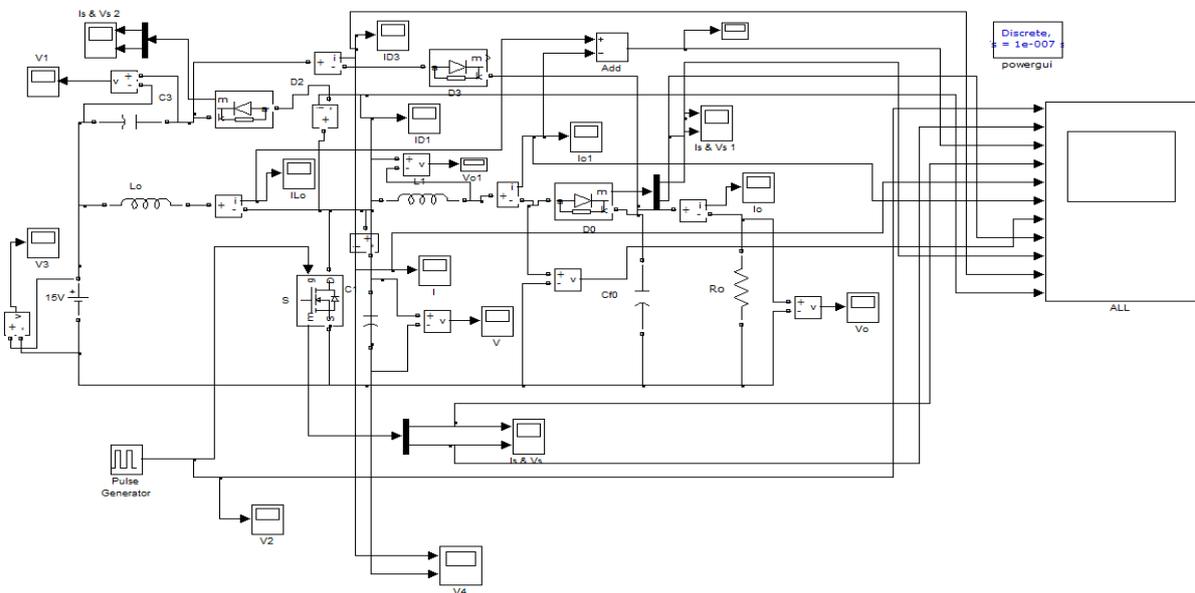


Fig. 9 Simulink Model

## VI. RESULT AND DISCUSSION

The gating pulses are generated at 0.36 duty ratio by pulse generator. This pulse is given to the gate of power switch. Gating pulses are shown in Fig. 10.

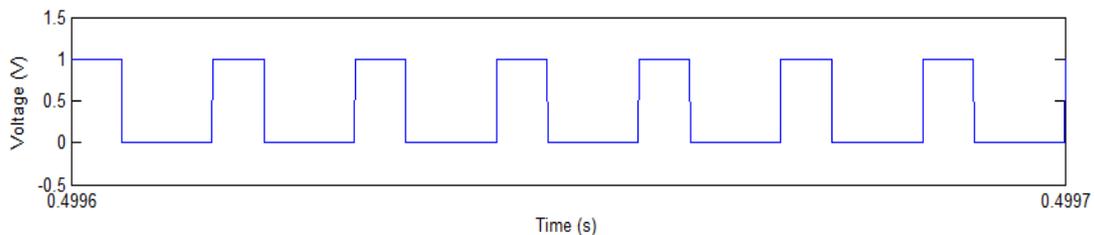


Fig. 10 Gating Pulse

The input to the converter is 15 V which is shown in Fig. 11. The input is steady and ripple free. The input source can be renewable energy sources or battery.

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 8, August 2015

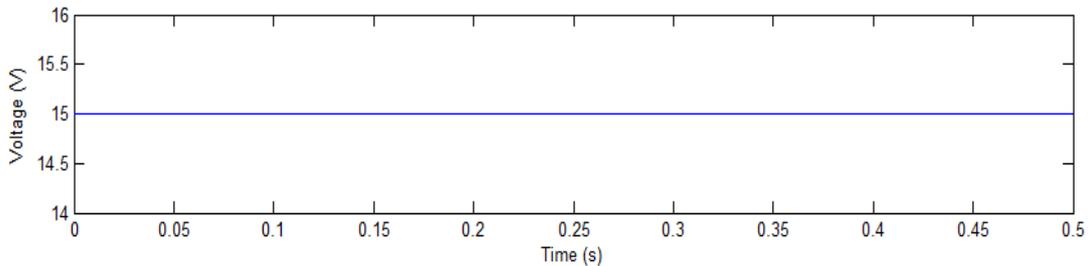


Fig. 11 Input Voltage

Fig. 12 shows the voltage across the switch. From the figure, it is clear that the switch transition occurs at zero voltage. Hence we can say that lossless switching is achieved .

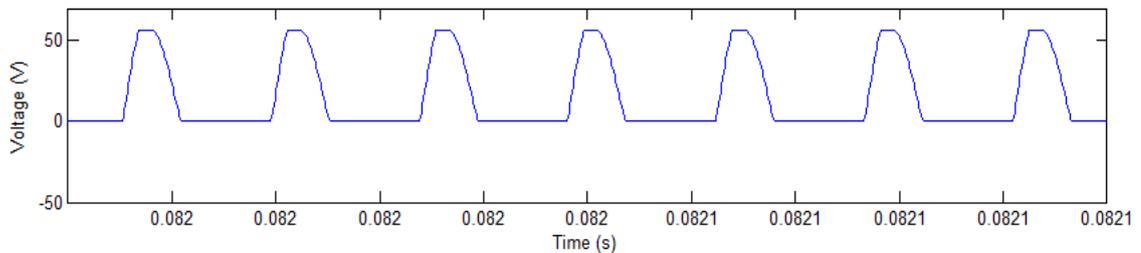


Fig. 12 Voltage across switch

Fig. 13 shows the current through the switch. From the figure, it is clear that the switch transition occurs at zero current. Maximum current through the switch is limited below 5A.

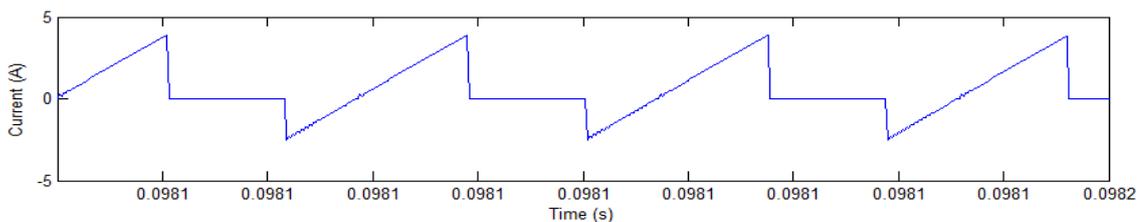


Fig. 13 Current through the switch

Fig. 14 shows the resonant capacitor current. Resonant transition of inductor capacitor pair is clear from this current waveform.

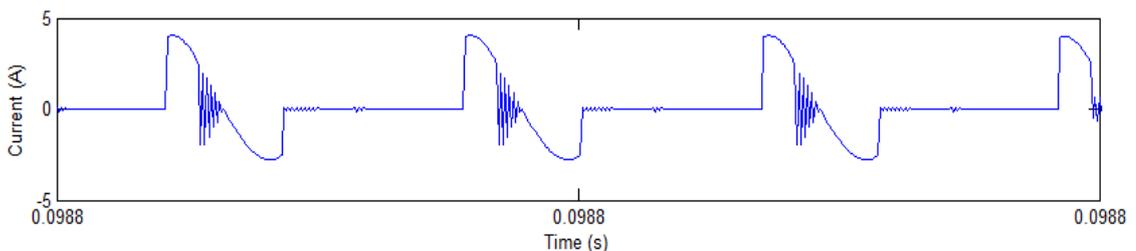


Fig. 14 Resonant capacitor current waveform

Fig. 15 shows the current through energy blocking diode. This figure reveals that this diode is operating under the ZCS condition, which can reduce the switching loss and increase the energy conversion efficiency.

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(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 8, August 2015

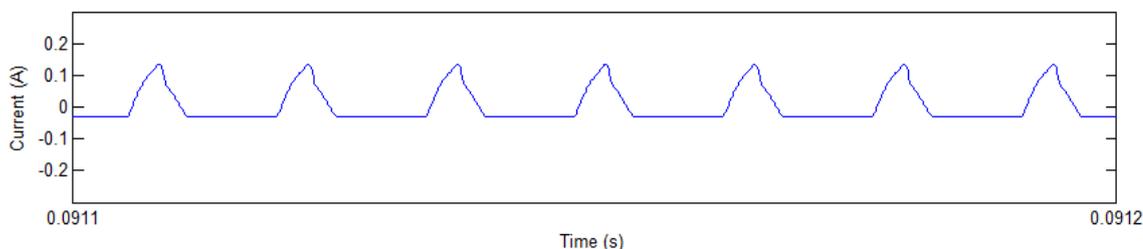


Fig. 15 Current through energy blocking diode

For an input voltage of 15V, the output voltage is boosted to 55V with a single switch converter which operated in zero voltage and zero current conditions. Fig. 16 shows the output voltage waveform.

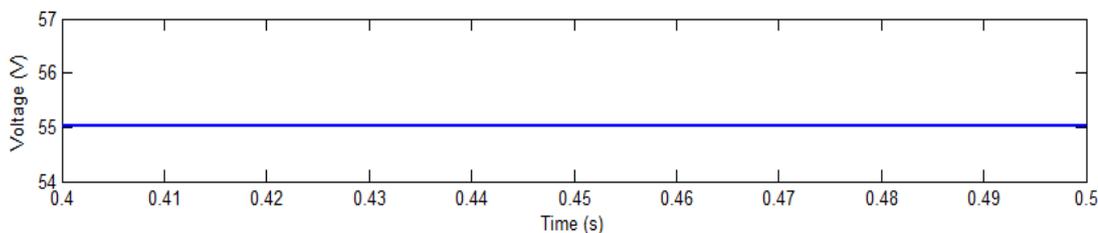


Fig. 16 Output Voltage

## VII.CONCLUSION

A novel ZVS step up converter has been designed for application in renewable energy generation systems. The main advantages of this converter includes soft switching, single switch operation, high voltage gain, less component count, low cost, minimum switching loss. The operation of circuit is analysed, and simulated the performance characteristics. The simulation results reveals the effectiveness of the developed novel ZVS step up converter in solar energy generation. For an input voltage of 15V, the output is 55V. ZVS and ZCS operation of switch is achieved. When the high-frequency converter is applied to a resistive load, high energy conversion efficiency is obtained.

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