



ISSN (Print) : 2320 – 3765
ISSN (Online): 2278 – 8875

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 10, October 2014

PV- FC Hybrid System and Its Power Management Strategies in a Grid

Chandan Kumar Tiwary ¹, Dr. Amita Mohar ²

PG Student, Dept. of Electrical & Electronics Engineering, NRI Institute of I.Sc. & Tech. Bhopal(M.P), India ¹

Professor & Head Dept. of Electrical & Electronics Engineering, NRI Institute of I.Sc. & Tech. Bhopal(M.P), India ²

ABSTRACT: This paper shows the work done on the method to operate a grid connected hybrid system which is composed of a Photovoltaic (PV) array and a Proton exchange membrane fuel cell .With the proton exchange membrane the hybrid system output power becomes controllable. Here the system uses two operation modes, the unit-power control (UPC) mode and the feeder-flow control (FFC) mode. This papers discusses the coordination of two control modes, the coordination of the PV array and the proton exchange membrane fuel cell in hybrid system and the way in which the reference parameters are determined. The proposed operating strategy with a flexible operation mode change always operates the The PV array operates at maximum output power and the Proton Exchange membrane cell in its high efficiency performance band, using the proposed strategy which has a flexible operation mode thus improving the performance of system operation with enhance stability and reduction in number of operating mode change.

KEYWORDS: Distributed generation, fuel cell, hybrid system, microgrid, photovoltaic, power management.

I.INTRODUCTION

With the world economic development and growing demand for energy, the conventional energy sources have become increasingly unable to meet the world demand for the energy. Thus, it is important to explore more and better means of alternative energy sources like sunlight, wind and biomass. Photovoltaic energy is a source of interesting energy; it is renewable, inexhaustible and non-polluting, and it is more and more intensively used as energy sources in various applications [1]. In regard to endless importance of solar energy, it is worth saying that solar energy is a unique perspective solution for energy crisis. Meanwhile, despite all these advantages of solar energy, they do not present desirable efficiency [2], [3]. The main renewable sources are biomass, geothermal, hydro, photovoltaic, and wind. Photovoltaic (PV) power is expected to have the fastest annual growth rate having already shown a top growth rate of more than 50% in 2006 and 2007 [4]. PV power systems have the advantage that their installation is static (i.e. no moving parts), simple and quickly compared to other renewable sources. Thus, they have a longer lifetime span, (typically more than 20 years) [5]. Moreover, due to their low operational cost and maintenance, they provide a significant solution for powering remote areas. The photovoltaic (PV) used to harness the solar energy tends to become an uncontrollable source because of the use of maximum power point tracking (MPPT) technique to continuously deliver the highest power to the load when variations in irradiation and temperature occur. The disadvantage of PV energy is that the PV output power depends on weather conditions and cell temperature, making it an uncontrollable source. Furthermore, it is not available during the night. In order to overcome these inherent drawbacks, alternative sources, such as PEMFC, should be installed in the hybrid system. By changing the FC output power, the hybrid source output becomes controllable. However, PEMFC, in its turn, works only at a high efficiency within a specific power range.

The hybrid system can either be connected to the main grid or work autonomously with respect to the grid connected mode or islanded mode, respectively. In the grid-connected mode, the hybrid source is connected to the main grid at the point of common coupling (PCC) to deliver power to the load. When load demand changes, the power supplied by the main grid and hybrid system must be properly changed. The power delivered from the main grid and PV array as well as PEMFC must be coordinated to meet load demand. The hybrid source has two control modes: 1) unit-power control (UPC) mode and feeder-flow control (FFC) mode. In the UPC mode, variations of load demand are compensated by the main grid because the hybrid source output is regulated to reference power. Therefore, the reference value of the hybrid

10.15662/ijareeie.2014.0310031

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 10, October 2014

source output must be determined. In the FFC mode, the feeder flow is regulated to a constant, the extra load demand is picked up by the hybrid source, and, hence, the feeder reference power must be known.

The proposed operating strategy is to coordinate the two control modes and determine the reference values of the UPC mode and FFC mode so that all constraints are satisfied. This operating strategy will minimize the number of operating mode changes, improve performance of the system operation, and enhance system stability.

II. SCHEME DETAILS

Structure of Grid-Connected Hybrid Power System

The system consists of a PV-FC hybrid source with the main grid connecting to loads at the PCC as shown in Fig. 1. The photovoltaic [8], [9] and the PEMFC [10], [11] are modeled as nonlinear voltage sources. These sources are connected to dc-dc converters which are coupled at the dc side of a dc/ac inverter. The dc/dc connected to the PV array works as an MPPT controller. Many MPPT algorithms have been proposed in the literature, such as incremental conductance (INC), constant voltage (CV), and perturbation and observation (P&O).

The P&O method has been widely used because of its simple feedback structure and fewer measured parameters [12]. The P&O algorithm with power feedback control [13]–[15] is shown in Fig. 2. As PV voltage and current are determined, the power is calculated. At the maximum power point, the derivative dP/dV is equal to zero. The maximum power point can be achieved by changing the reference voltage by the amount of ΔV_{ref} .

Photovoltaic Array Model

The mathematical model 3 and 4 can be expressed as

$$I = I_{ph} - I_{sat} \left\{ \exp \left[\frac{q}{AKT} (V + IR_s) \right] - 1 \right\}. \quad (1)$$

Equation (1) shows that the output characteristic of a solar cell is nonlinear and vitally affected by solar radiation, temperature, and load condition. Photocurrent I_{ph} is directly proportional to solar radiation G_a .

$$I_{ph}(G_a) = I_{sc} \frac{G_a}{G_{as}}. \quad (2)$$

The short-circuit current of solar cell I_{sc} depends linearly on cell temperature

$$I_{sc}(T) = I_{scs}[1 + \Delta I_{sc}(T - T_s)]. \quad (3)$$

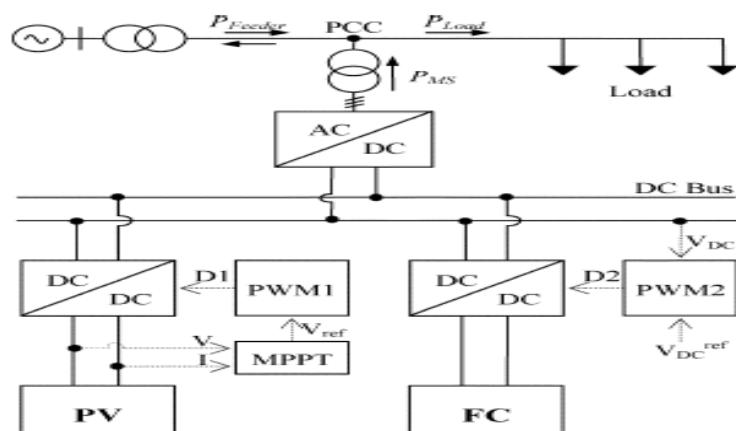


Figure 1 PV-FC Hybrid system employed in a grid

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 10, October 2014

Thus, I_{ph} depends on solar irradiance and cell temperature

$$I_{ph}(G_a, T) = I_{scs} \frac{G_a}{G_{as}} [1 + \Delta I_{sc}(T - T_s)]. \quad (4)$$

I_{sat} also depends on solar irradiation and cell temperature and can be mathematically expressed as follows:

$$I_{sat}(G_a, T) = \frac{I_{ph}(G_a, T)}{e^{\left(\frac{V_{oc}(T)}{V_t(T)}\right)} - 1}. \quad (5)$$

PEMFC Model

The PEMFC steady-state feature of a PEMFC source is assessed by means of a polarization curve, which shows the nonlinear relationship between the voltage and current density. The PEMFC output voltage is as follows [10]:

$$V_{out} = E_{Nerst} - V_{Act} - V_{ohm} - V_{conc} \quad (6)$$

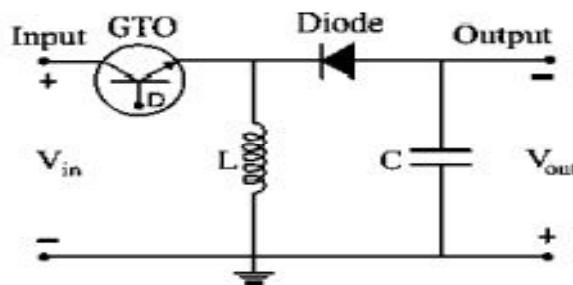


Figure 3 Buck Boost topology

where E_{Nerst} is the “thermodynamic potential” of Nerst, which represents the reversible (or open-circuit) voltage of the fuel cell. Activation voltage drop V_{Act} is given in the Tafel equation as

$$V_{act} = T[a + b \ln(I)] \quad (7)$$

where a, b are the constant terms in the Tafel equation (in volts per Kelvin). The overall ohmic voltage drop V_{ohm} can be expressed as

$$V_{ohm} = I R_{ohm} \quad (8)$$

The ohmic resistance R_{ohm} of PEMFC consists of the resistance of the polymer membrane and electrodes, and the resistances of the electrodes. The concentration voltage drop V_{conc} is expressed as

$$V_{conc} = -\frac{RT}{zF} \ln \left(1 - \frac{I}{I_{limit}} \right). \quad (9)$$

MPPT Control

Many MPPT algorithms have been proposed in the literature, such as incremental conductance (INC), constant voltage (CV), and perturbation and observation (P&O). The two algorithms often used to achieve maximum power point tracking are the P&O and INC methods. The INC method offers good performance under rapidly changing atmospheric conditions. However, four sensors are required to perform the computations.

If the sensors require more conversion time, then the MPPT process will take longer to track the maximum power point. During tracking time, the PV output is less than its maximum power. This means that the longer the conversion time is, the larger amount of power loss [12] will be. On the contrary, if the execution speed of the P&O method



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 10, October 2014

increases, then the system loss will decrease. Moreover, this method only requires two sensors, which results in a reduction of hardware requirements and cost. Therefore, the P&O method is used to control the MPPT process.

In order to achieve maximum power, two different applied control methods that are often chosen are voltage-feedback control and power-feedback control [13], [14]. Voltage-feedback control uses the solar-array terminal voltage to control and keep the array operating near its maximum power point by regulating the array's voltage and matching the voltage of the array to a desired voltage. The drawback of the voltage-feedback control is its neglect of the effect of irradiation and cell temperature. Therefore, the power-feedback control is used to achieve maximum power.

The P&O MPPT algorithm with a power-feedback control [14], [15] is shown in Fig. 2. As PV voltage and current are determined, the power is calculated. At the maximum power point, the derivative (dP/dV) is equal to zero. The maximum power point can be achieved by changing the reference voltage by the amount of ΔV_{ref} . In order to implement the MPPT algorithm, a buck-boost dc/dc converter is used as depicted in Fig. 3. The parameters L and C in the buck-boost converter must satisfy the following conditions [16]:

$$L > \frac{(1-D)^2 R}{2f} ; \quad C > \frac{D}{R_f(\Delta V/V_{out})}. \quad (10)$$

The buck-boost converter consists of one switching device (GTO) that enables it to turn on and off depending on the applied gate signal D. The gate signal for the GTO can be obtained by comparing the sawtooth waveform with the control voltage [12]. The change of the reference voltage ΔV_{ref} obtained by MPPT algorithm becomes the input of the pulsedwidth modulation (PWM). The PWM generates a gate signal to control the buck-boost converter and, thus, maximum power is tracked and delivered to the ac side via a dc/ac inverter.

III. CONTROL OF THE HYBRID SYSTEM

Unit power control, feeder flow control, and mixed control mode are the control modes used in microgrid. In the UPC mode, the DGs (the hybrid source in this system) regulate the voltage magnitude at the connection point and the power that source is injecting. In this mode if a load increases anywhere in the microgrid, the extra power comes from the grid, since the hybrid source regulates to a constant power. In the FFC mode, the DGs regulate the voltage magnitude at the connection point and the power that is flowing in the feeder at connection point P_{feeder} . With this control mode, extra load demands are picked up by the DGs, which maintain a constant load from the utility viewpoint.

In this paper, a coordination of the UPC mode and the FFC mode was investigated to determine when each of the two control modes was applied and to determine a reference value for each mode. With both the sources having their constraints the reference power must be set at an appropriate value so that the constraints of these sources are satisfied.

IV. OPERATING STRATEGY OF THE HYBRID SYSTEM

As mentioned before, the purpose of the operating algorithm is to determine the control mode of the hybrid source and the reference value for each control mode so that the PV is able to work at maximum output power and the constraints are fulfilled. Once the constraints (P_{FC}^{low} , P_{FC}^{up} , P_{FC}^{max} , P_{MS}^{Ref}) are known, the control mode of the hybrid source (UPC mode and FFC mode) depends on load variations and the PV output. In the UPC mode, the reference output power of the hybrid source P_{MS}^{Ref} depends on the PV output and the constraints of the FC output.



ISSN (Print) : 2320 – 3765
ISSN (Online): 2278 – 8875

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 10, October 2014

V. RESULT AND DISCUSSION

Simulation results without Hysteresis

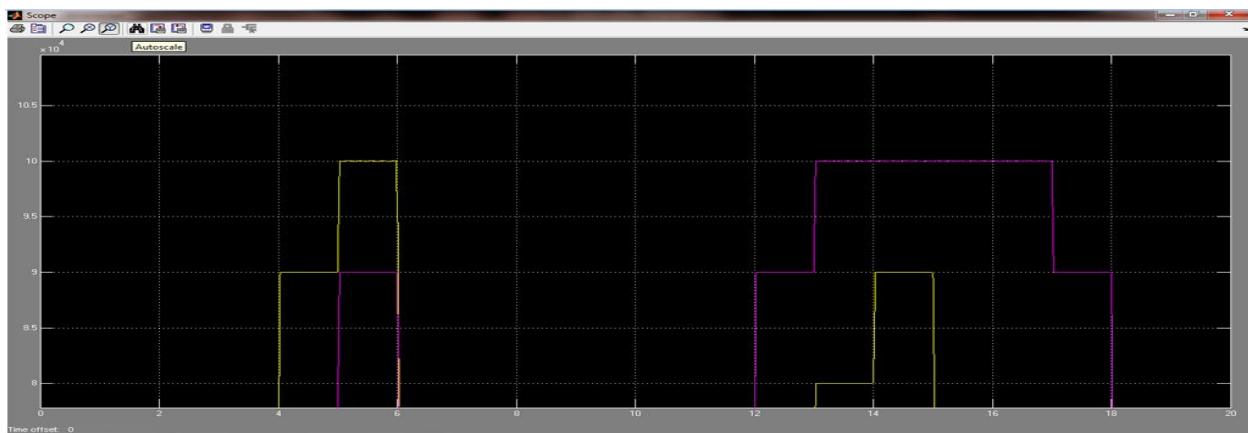


Figure 4 Operating strategy of the operating source without hysteresis

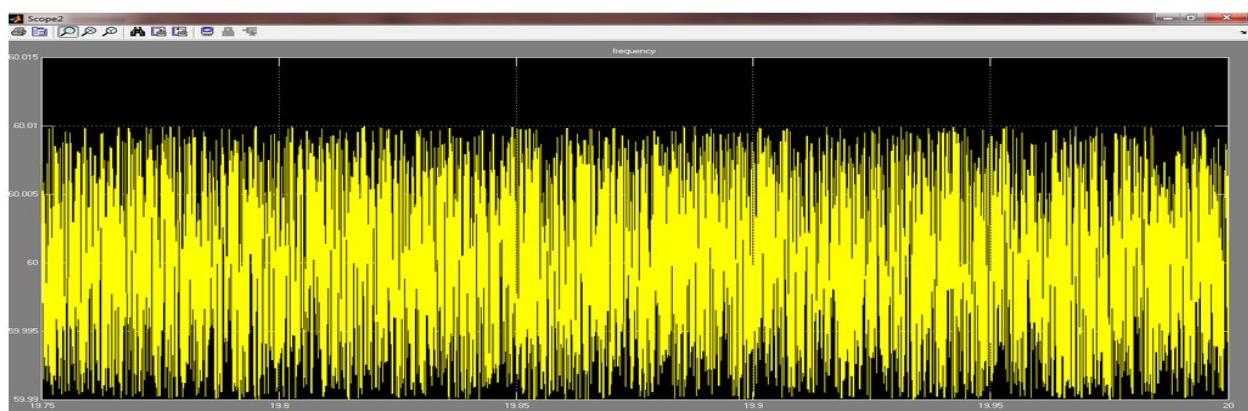


Figure 5 Frequency variation in the system



Figure 6 Change of operating modes

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 10, October 2014

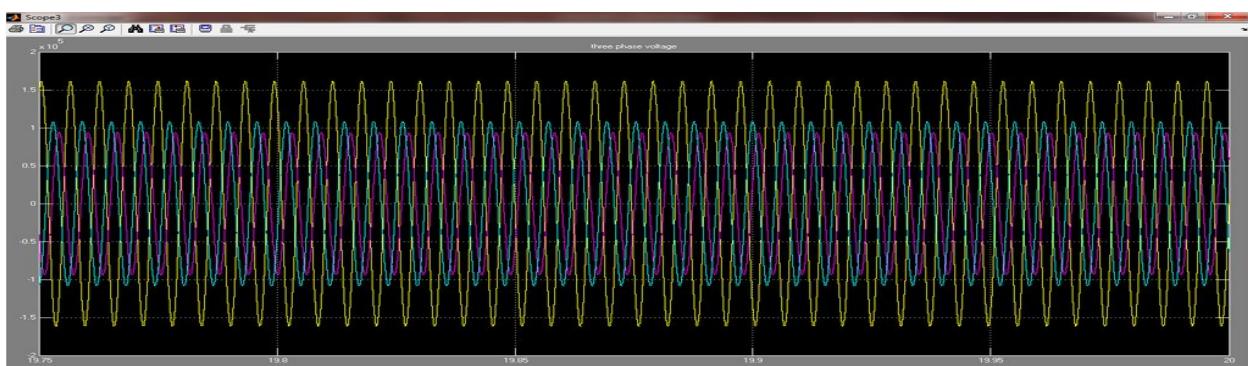


Figure 7 Three phase voltage of the system

Output With Hysteresis

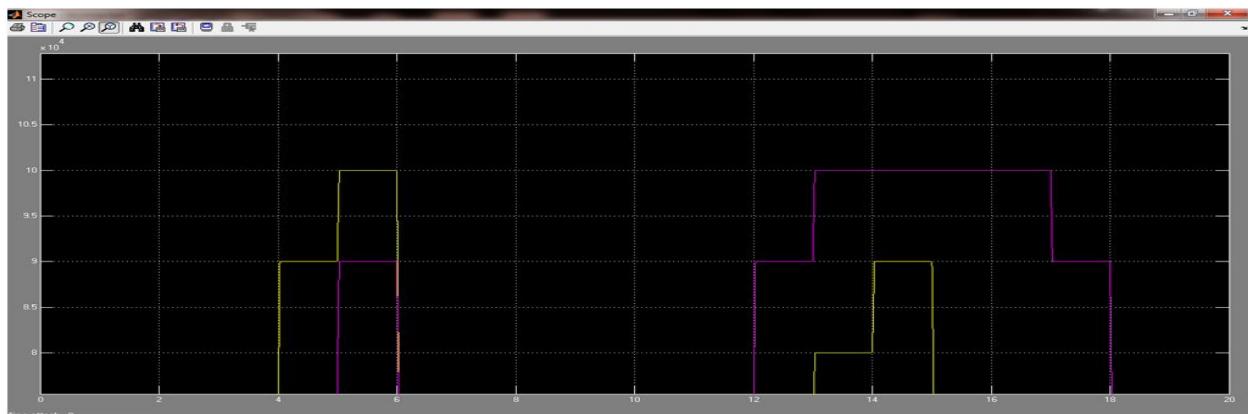


Figure 4 Operating strategy of the operating source with hysteresis

We observe that between $t=13$ sec to $t = 17$ sec the output shows glitches when we are using the system without hysteresis but when we are using hysteresis we are able to reduce the glitches between $t=13$ sec to $t = 17$ sec. We can also make the conclusion that the system frequency remains well within the specified range

VI.CONCLUSION

In this paper we have been able to present an available method to operate a hybrid grid-connected system which is composed of a PV array and PEMFC with hysteresis and without hysteresis. The operating strategy of the system is based on the UPC mode and FFC mode. The purpose for going for this particular strategy is to determine the control mode, to minimize the number of mode changes, to operate PV at the maximum power point, and to operate the FC output in its high-efficiency performance band.

In brief, the proposed algorithm presents a simplified and flexible method to operate a hybrid source in a grid-connected microgrid which can improve the performance of the system's operation and thus allows the system to work more stably while maximizing the PV output power.

Future work may involve considering the operation of the battery into account to enhance operation performance of the system. Work may also be carried to study the application of the operating algorithm to a microgrid with multiple feeders and DGs will also be studied in detail.



ISSN (Print) : 2320 – 3765
ISSN (Online): 2278 – 8875

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 10, October 2014

REFERENCES

- [1] H Zang and X Yang. "Simulation and analysis of two-level photovoltaic grid-connected system". vol. 433-440, ed, 2012, pp. 1406-1411.
- [2] C González-Morán, et al. "Improved model of photovoltaic sources considering ambient temperature and solar irradiation". 2009.
- [3] T Kerzmann and L Schaefer. "System simulation of a linear concentrating photovoltaic system with an active cooling system". Renewable Energy. vol. 41, pp. 254-261, 2012.
- [4] AR Di Fazio and M Russo. "Photovoltaic generator modeling to improve numerical robustness of EMT simulation". Electric Power Systems Research. vol. 83, pp. 136-143, 2012.
- [5] Z Wang, et al. "Modeling of arbitrary power level PV array based on a circuit equivalent mechanism". vol. 424-425, ed, 2012, pp. 586-591. T. Bocklisch, W. Schüff, and S. Bocklisch, "Predictive and optimizing energy management of photovoltaic fuel cell hybrid systems with shorttime energy storage," in *Proc. 4th Eur. Conf. PV-Hybrid and MiniGrid*, 2008, pp. 8–15.
- [6] J. Larmine and A. Dicks, *Fuel Cell Systems Explained*. New York: Wiley, 2003.
- [7] W. Xiao, W. Dunford, and A. Capel, "A novel modeling method for photovoltaic cells," in *Proc. IEEE 35th Annu. Power Electronics Specialists Conf.*, Jun. 2004, vol. 3, pp. 1950–1956.
- [8] D. Sera, R. Teodorescu, and P. Rodriguez, "PV panel model based on datasheet values," in *Proc. IEEE Int. Symp. Industrial Electronics*, Jun.4–7, 2007, pp. 2392–2396.
- [9] C. Wang, M. H. Nehrir, and S. R. Shaw, "Dynamic models and model validation for PEM fuel cells using electrical circuits," *IEEE Trans. Energy Convers.*, vol. 20, no. 2, pp. 442–451, Jun. 2005.
- [10] C. Hua and C. Shen, "Comparative study of peak power tracking techniques for solar storage system," in *Proc. 13th Annu. Applied Power Electronics Conf. Expo.*, Feb. 1998, vol. 2, pp. 679–685.
- [11] A. Hajizadeh and M. A. Golkar, "Power flow control of grid-connected fuel cell distributed generation systems," *J. Elect. Eng. Technol.*, vol.3, no. 2, pp. 143–151, 2008.
- [12] C. Hua and J. R. Lin, "DSP-based controller application in battery storage of photovoltaic system," in *Proc.22nd IEEE Int. Conf. IndustrialElectronics, Control, and Instrumentation*, Aug. 5–10, 1996, vol. 3, pp. 1750–1810.
- [13] C. Hua, J. Lin, and C. Shen, "Implementation of a DSP-controlled photovoltaic system with peak power tracking," *IEEE Trans. Ind. Electron.*, vol. 45, no. 1, pp. 99–107, Feb. 1998.
- [14] E. Koutroulis and K. Kaalitzakis, "Development of a microcontroller based, photovoltaic maximum power point tracking control system," *IEEE Trans. Power Electron.*, vol. 16, no. 1, pp. 46–54, Jan. 2001.
- [15] N. Mohan, T. M. Undeland, and W. P. Robbins, *Power Electronics, Converters, Applications and Design*, 2nd ed. New York: Wiley, 2003.
- [16] R. H. Lasseter, "Microgrids," in *Proc. IEEE Power Eng. Soc. Winter Meeting*, Jan. 2002, vol. 1, pp. 305–308.
- [17] R. H. Lasseter and P. Piagi, "Control and design of microgrid components," Jan. 2006, PSERC final project reports.
- [18] P. Piagi and R. H. Lasseter, "Autonomous control of microgrids," presented at the Power IEEE Eng. Soc. General Meeting, Montreal, QC,Canada, 2006.
- [19] F. Katiraei and M. R. Iravani, "Power management strategies for a microgrid with multiple distributed generation units," *IEEE Trans. Power Syst.*, vol. 21, no. 4, pp. 1821–1831, Nov. 2006. [16] J. A. Peças Lopes, C. L. Moreira, and A. G. Madureira, "Defining control strategies for microgrids islanded operation," *IEEE Trans. Power Syst.*, vol. 21, no. 2, pp. 916–924, May 2006.
- [20] H. Jiayi, J. Chuanwn, and X. Rong, "A review on distributed energy resources and microgrid," *Renew. Sustain. Energy Rev.*, vol. 12, pp.2472–2483, 2008.
- [21] M. Barnes, G. Ventakaramanan, J. Kondoh, R. Lasseter, H. Asano, N. Hatziargyriou, J. Oyarzabal, and T. Green, "Real-world microgrids—An overview," in *Proc. IEEE Int. Conf. System of Systems Engineering*, Apr. 16–18, 2007, pp. 1–8.
- [22] Loc Nguyen Khanh, Jae-Jin Seo, Yun-Seong Kim, and Dong-Jun Won, "Power-Management Strategies for a Grid-Connected PV-FC Hybrid System" in *IEEE Transactions on Power Delivery*, Vol. 25, NO. 3, July 2010.